



Influence of Sulfate Reduction and Biogenic Reactive Minerals on Long-Term PRB Performance in a Sulfate Rich, High Flow Aquifer

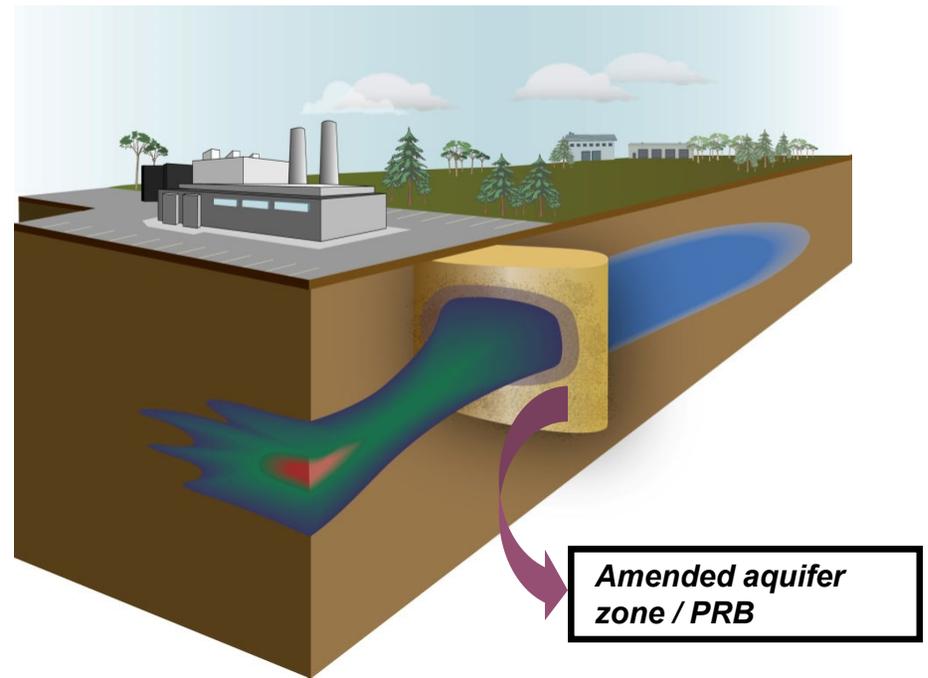
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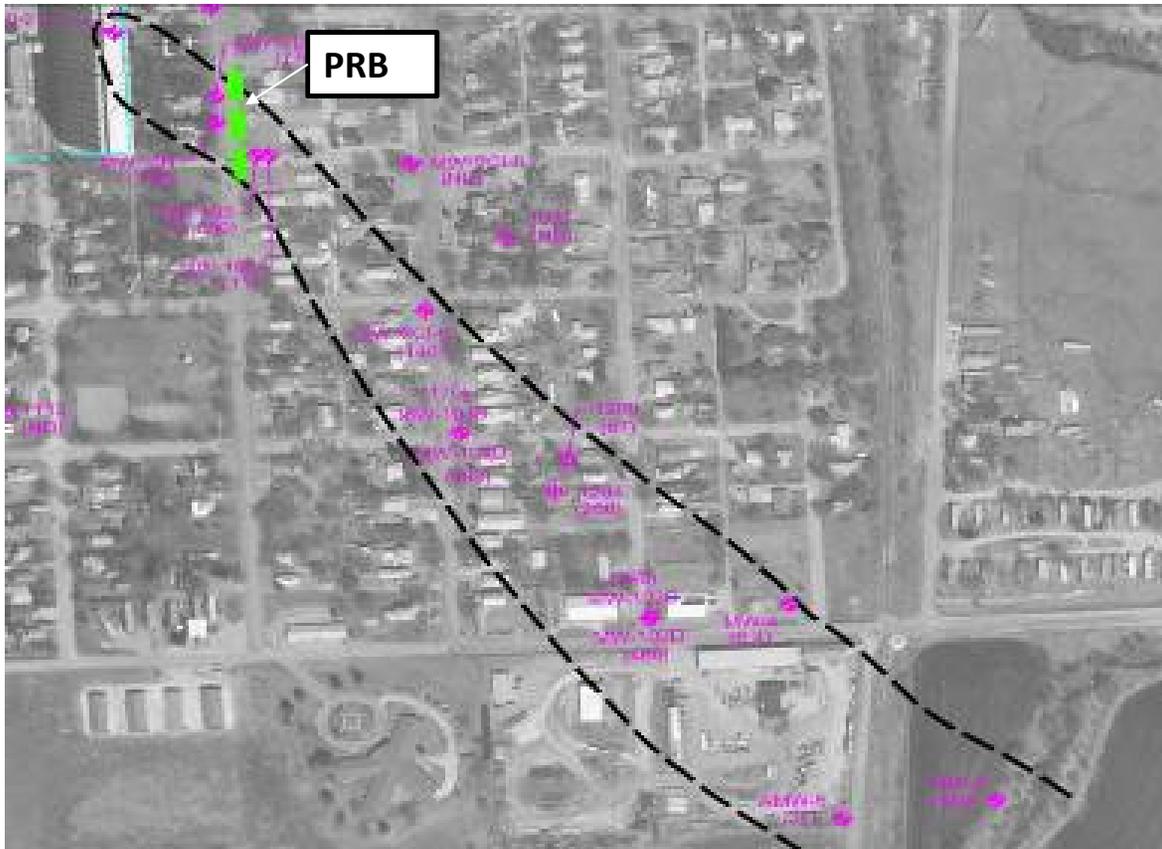
Fifth International Symposium on Bioremediation and Sustainable Environmental Technologies
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Introduction

- EHC PRB installed in 2005 for treatment of carbon tetrachloride (CT)
- One of the first full-scale applications of ISCR reagents into an injection PRB
- The objective with this presentation is to assess long-term performance and changes to geochemical parameters since installation



Remedial Approach



- ❖ Remedial approach developed by Malcolm Pirnie (Arcadis)
- ❖ In April 2005, a PRB was installed across the width of the plume downgradient from the source to limit further plume migration.
- ❖ It was installed along the first available roadway by injecting EHC ISCR reagents into a line of direct push injection points.

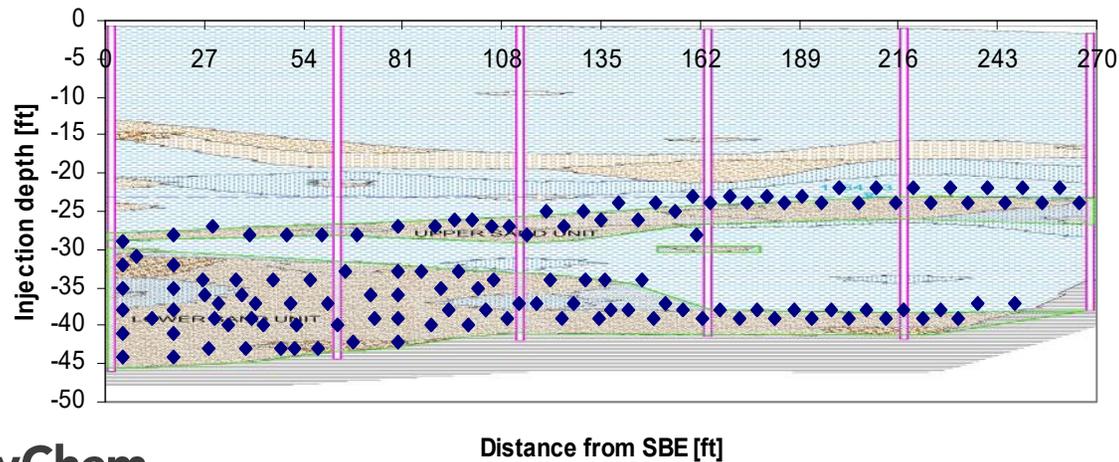
Reagent Selection

- EHC selected over straight ZVI following bench scale testing due to its ability to more effectively treat CT break down products.
- Rapid abiotic CT degradation with ZVI alone, but a portion of the CT is converted to CF and a portion of the CF is converted to DCM
- EHC[®] ISCR reagent composed of:
 - 40% micro-scale ZVI (50 - 150 μm)
 - 60% fine-grained processed plant fiber particles
- EHC promotes both abiotic and biotic degradation mechanisms



PRB installation via DPT injection

- EHC PRB installed as a line of DPT injection points across the width of the plume
- Upper and lower sand unit targeted for injection
- PRB Dimensions: 270 ft long x 15 ft wide x 10 ft deep on average
- A total of 24 tons of EHC injected
- EHC Application Rate = ca 1% to soil mass



Evaluation of EHC Placement

Soil cores obtained at the beginning of the installation to verify radius of influence and determine injection spacing:

- EHC slurry was found to distribute in discrete seams and detected 5 ft away from the injection location
- Injection points spaced 10 ft apart



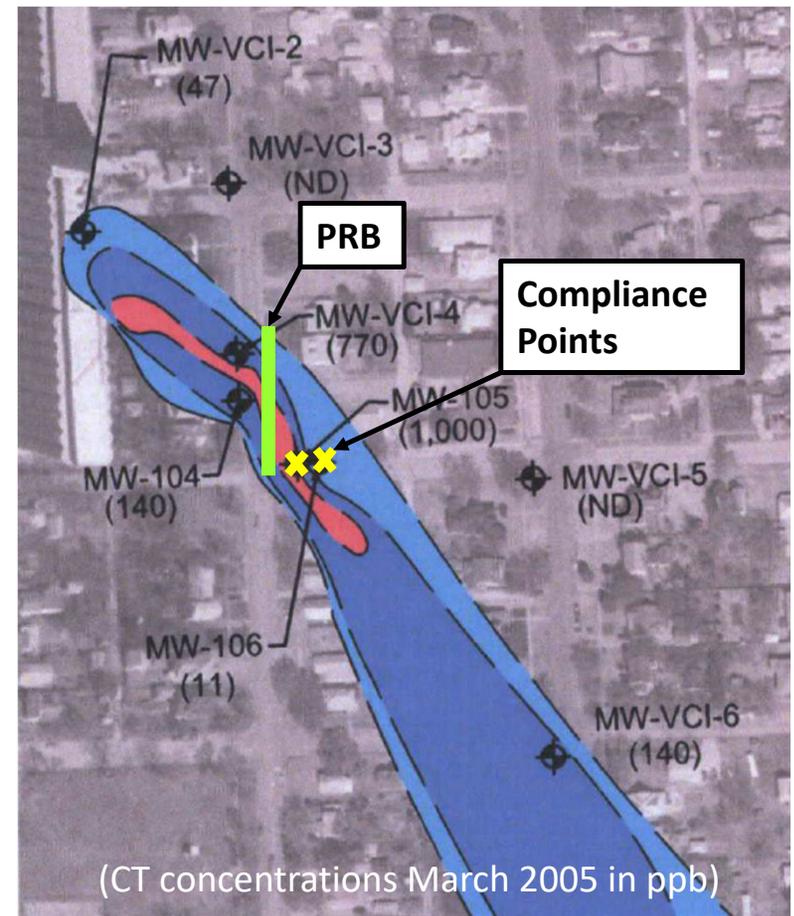
Horizontal fracture



Vertically dipping fracture

PRB Performance Evaluation

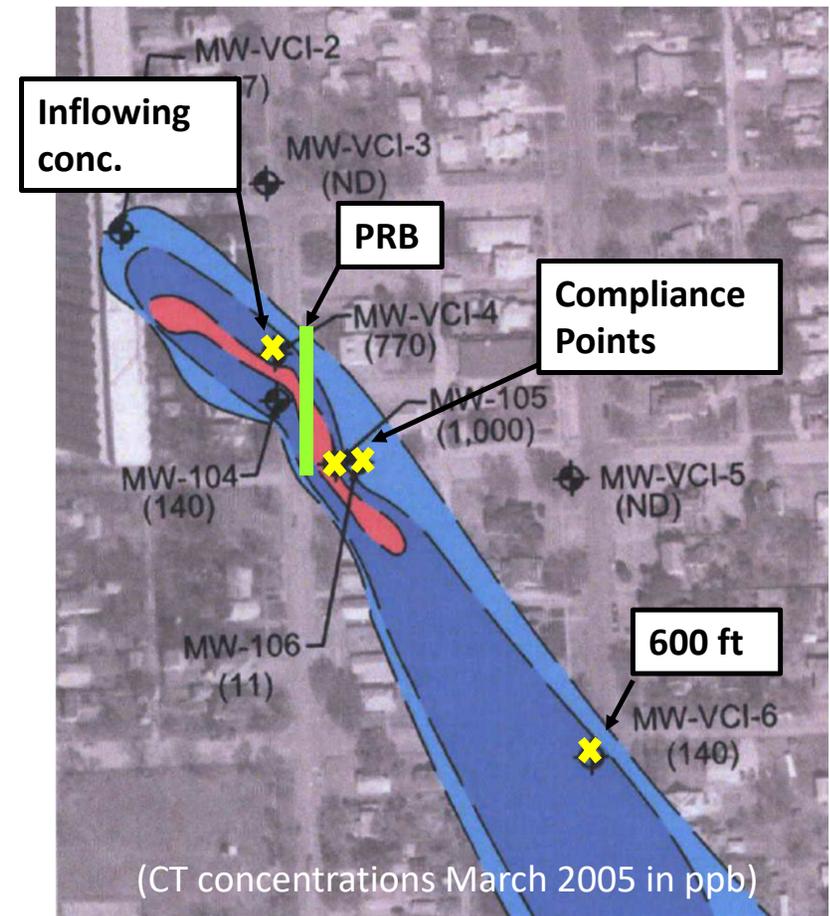
- ❖ **Remedial goal:** Maintain a removal efficiency of at least **95% reduction** in CT compared to baseline concentrations at compliance points located 70 and 140 ft downgradient from the PRB.



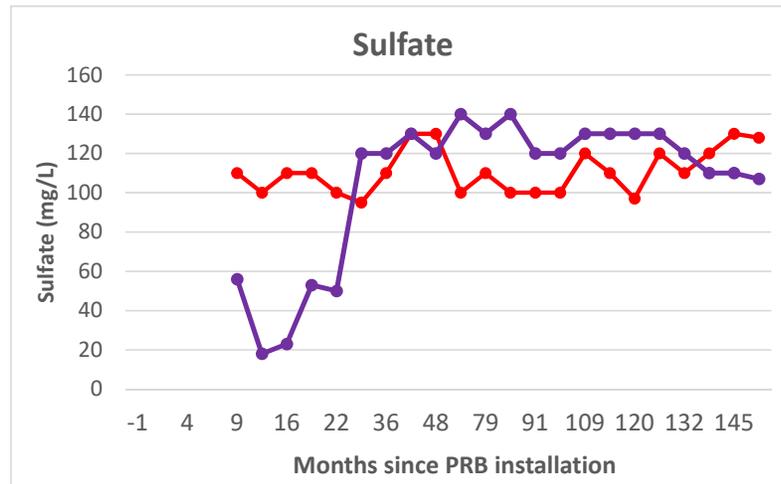
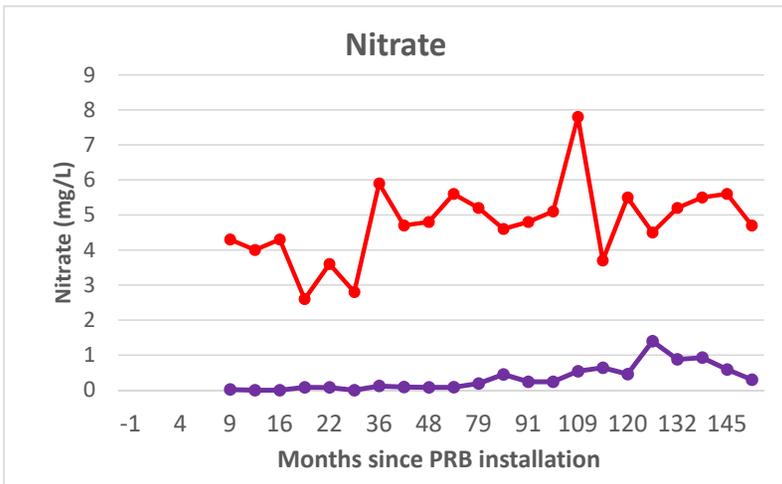
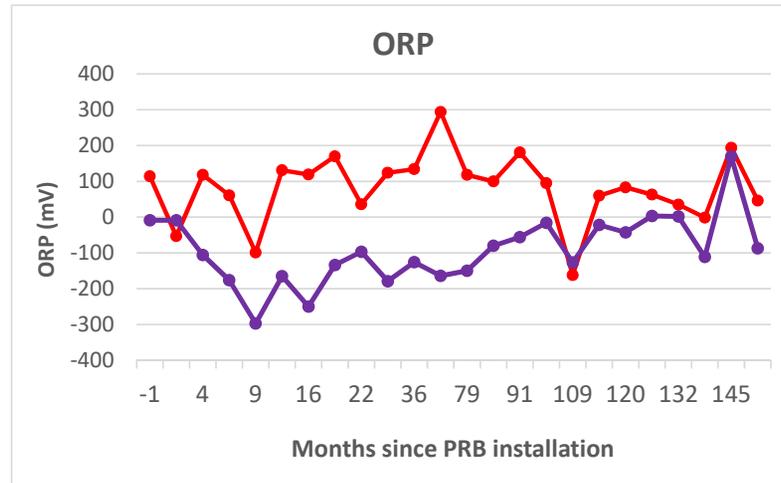
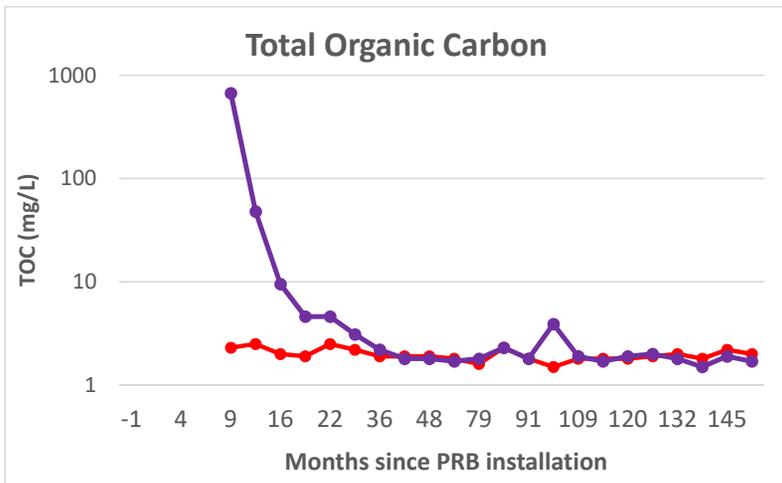
PRB Performance Evaluation

- ❖ **MW-105** - 70 ft downgradient at center of plume / ~39 days gw travel time*
- ❖ **MW-106** - 140 ft downgradient at edge of plume / ~78 days gw travel time*
- ❖ **MW-VCI-6** - 600 ft downgradient / ~333 days gw travel time*
- ❖ Inflowing concentrations monitored at **MW-VCI-4**

*based on an estimated **gw flow velocity of 1.8 ft/day**

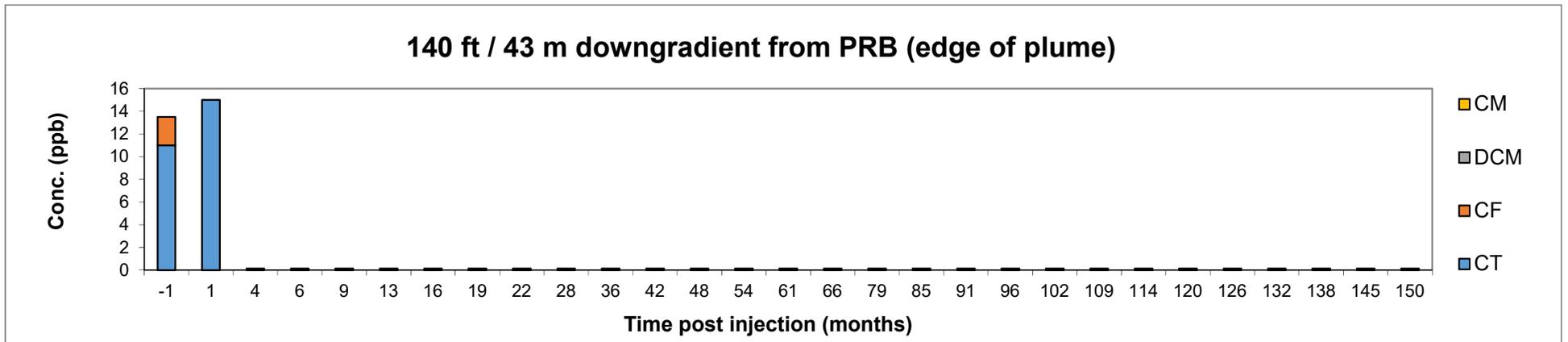
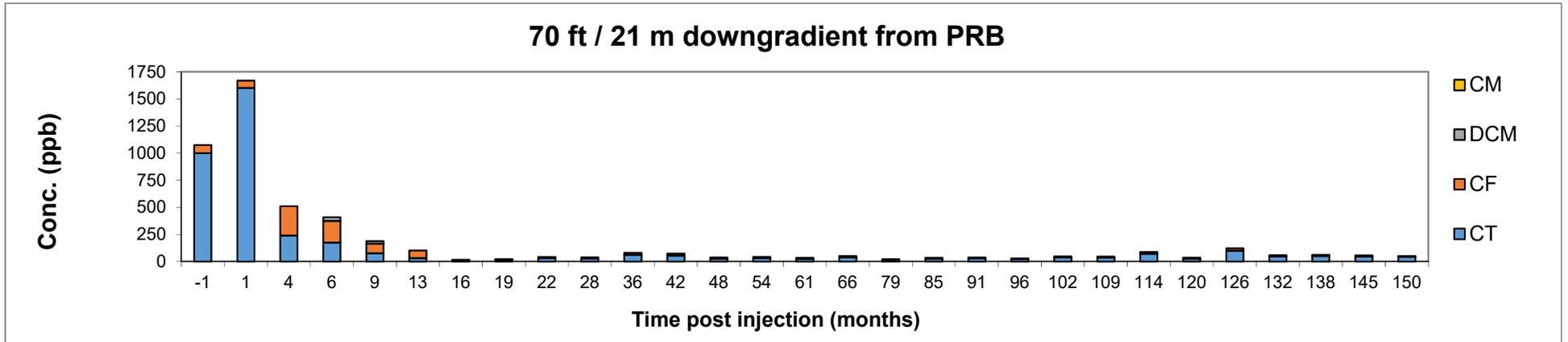


Geochemical Response – 12.5 years



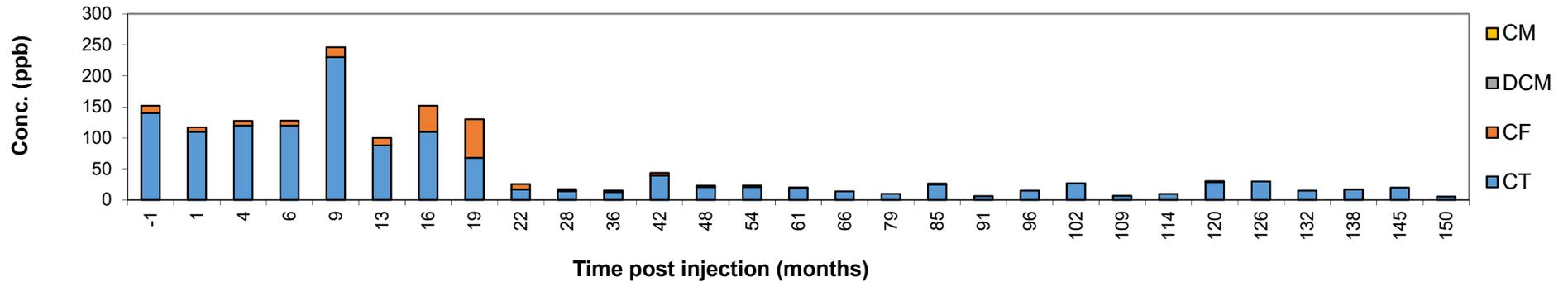
- MW-VCL4 (upgradient / inflowing)
- MW-105 (21 m downgradient)

Performance Data

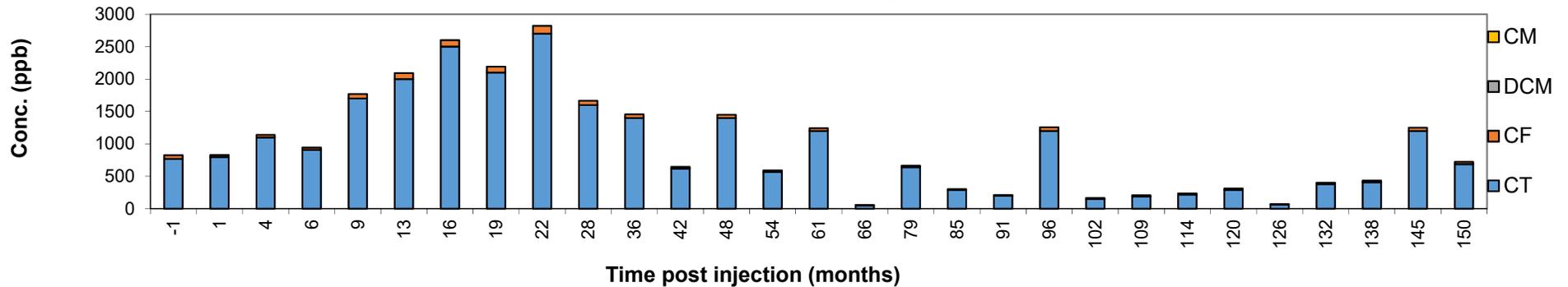


Performance Data

600 ft / 183 m downgradient from PRB



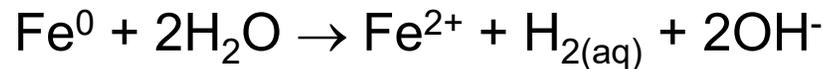
Inflowing concentrations measured 85 ft / 26 m upgradient of PRB



Micro-Scale ZVI Longevity

Theoretical estimation of micro-scale ZVI longevity:

- **ZVI oxidation** due to reduction of terminal electron acceptors; calculated based on Stoichiometric demand from:
 - Naturally occurring terminal electron acceptors such as dissolved oxygen (DO), nitrate and sulfate;
 - Chlorinated contaminant reduction.
- **Corrosion** is an important ZVI consumption process and rates are expected to be more constant over time (estimated at 0.8 mmol/kg/day for micro-scale ZVI):



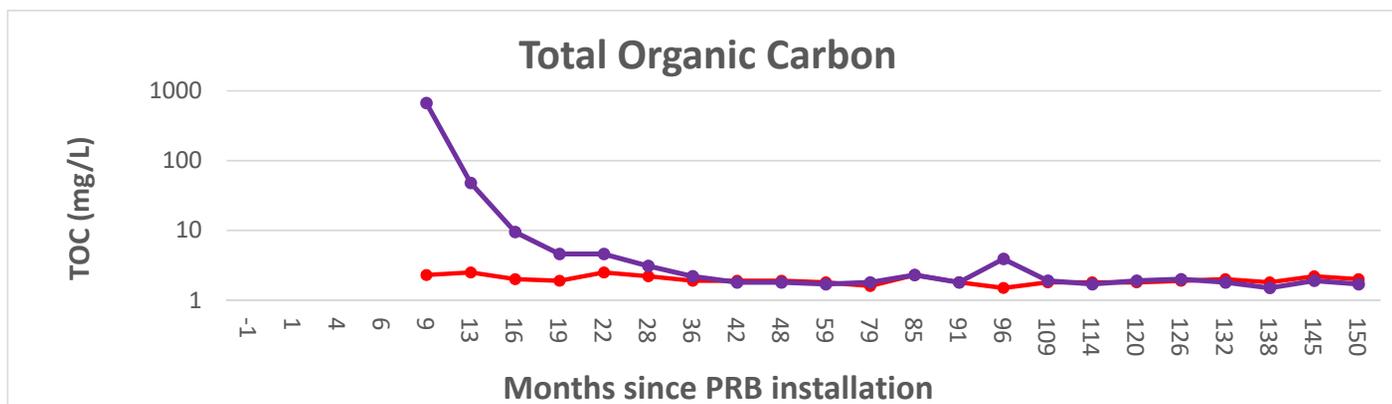
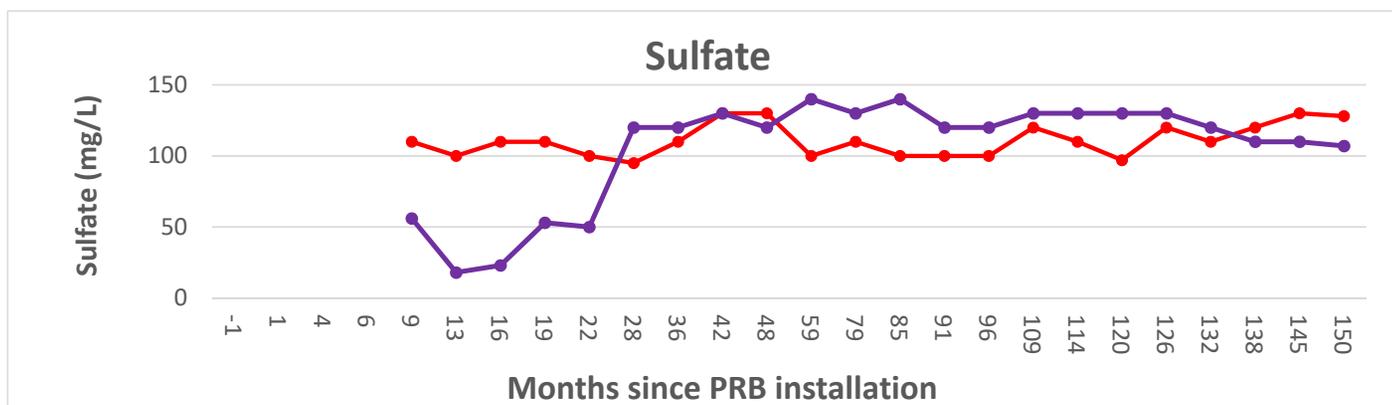
Theoretical Calculation of ZVI Longevity

PRB interface for gw flow (m2)	PRB width (m)	ZVI Dose Rate (mass)	ZVI Mass (kg)	GW velocity (m/day)	Effective porosity	Volume gw passing thru PRB (L/yr)
251	4.6	0.4%	8709	0.55	15%	7,534,688

Estimation assuming 100% of inflowing sulfate being reduced:

	Influent (mg/L)	Mass flux (kg/yr)	Mass flux (kmol/yr)	ZVI used (kmol/yr)	ZVI used (kg/yr)	% ZVI used per year
Water corrosion	---	---	---	---	142	1.6%
DO	0.4	3	94	126	7	0.1%
CT	1	8	49	98	5	0.1%
CF	0.01	0.8	6	6	0.4	0.004%
NO3	4	30	486	1,944	108	1.2%
SO4	120	904	9,418	37,673	2,102	24.1%
Total						27.2%
Estimated ZVI Longevity (yrs)						3.7

Sulfate Reduction vs. TOC



- MW-VCL4 (upgradient / inflowing)
- MW-105 (21 m downgradient)

Theoretical Calculation of ZVI Longevity

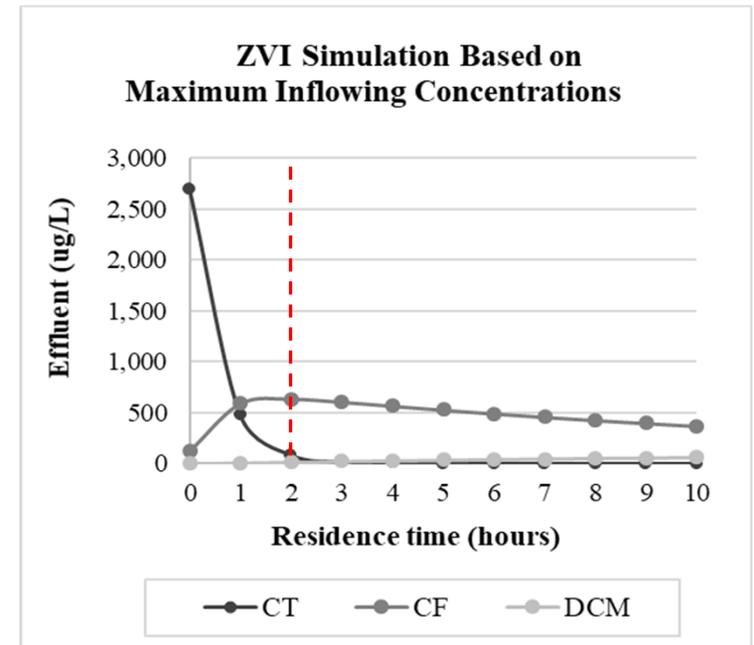
PRB interface for gw flow (m2)	PRB width (m)	ZVI Dose Rate (mass)	ZVI Mass (kg)	GW velocity (m/day)	Effective porosity	Volume gw passing thru PRB (L/yr)
251	4.6	0.4%	8709	0.55	15%	7,534,688

Estimation assuming no sulfate reduction from ZVI:

	Influent (mg/L)	Mass flux (kg/yr)	Mass flux (kmol/yr)	ZVI used (kmol/yr)	ZVI used (kg/yr)	% ZVI used per year
Water corrosion	---	---	---	---	142	1.6%
DO	0.4	3	94	126	7	0.1%
CT	1	8	49	98	5	0.1%
CF	0.01	0.8	6	6	0.4	0.004%
NO3	4	30	486	1,944	108	1.2%
SO4	-	-	-	-	-	-
Total						3.0%
Estimated ZVI Longevity (yrs)						33.1

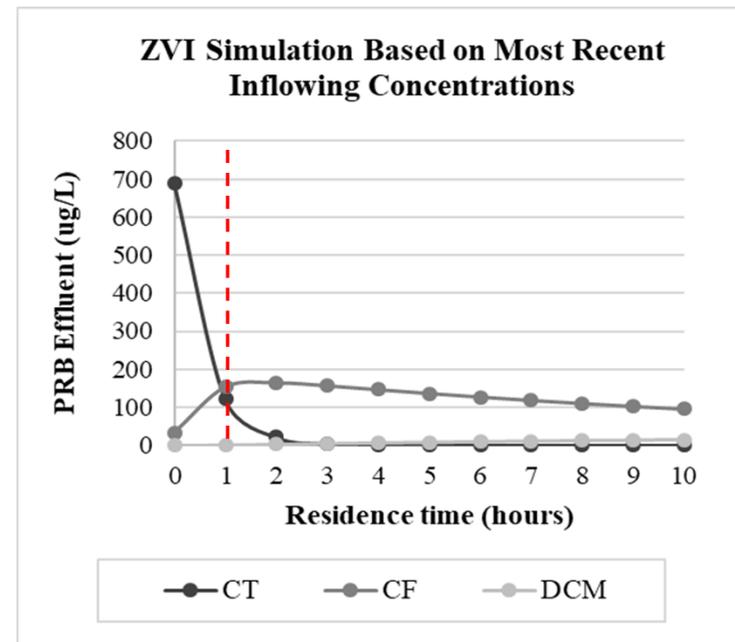
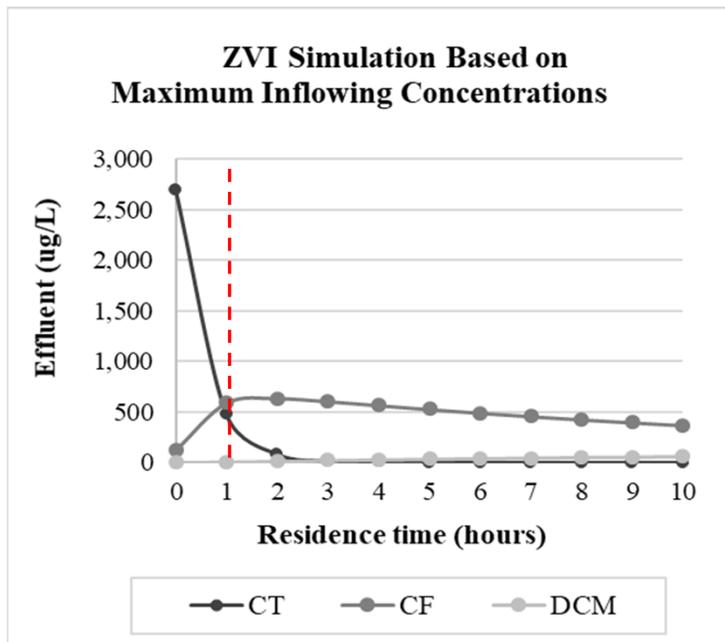
Simulated Effluent Concentrations

- Simulations performed based on ZVI only (assuming organic carbon mostly depleted)
- Effluent concentrations simulated using lab determined half life data (100% ZVI):
 - $CT_{1/2} = 0.4$ hours ; $CF_{1/2} = 9.6$ hours
 - Molar conversion: CT to CF: 29%; CF to DCM: 22%
- A residence time of ~2 hours required to achieve the goal of reducing CT by 95%:
 - Flow-through thickness of 0.15 ft (4.6 cm) of 100% ZVI required



Simulated Effluent Concentrations

- The EHC PRB contained an equivalent of 1.8 cm of 100% ZVI:
 - 0.4% ZVI distributed over a 15 ft PRB width
 - Equates to a residence time of <1 hour

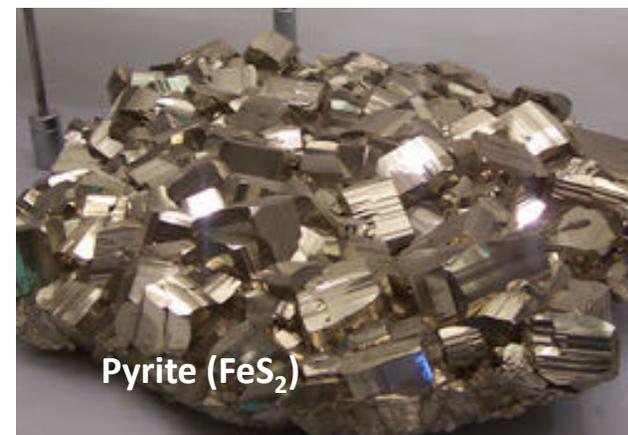


Simulated vs. Actual Effluent 1 hour residence time

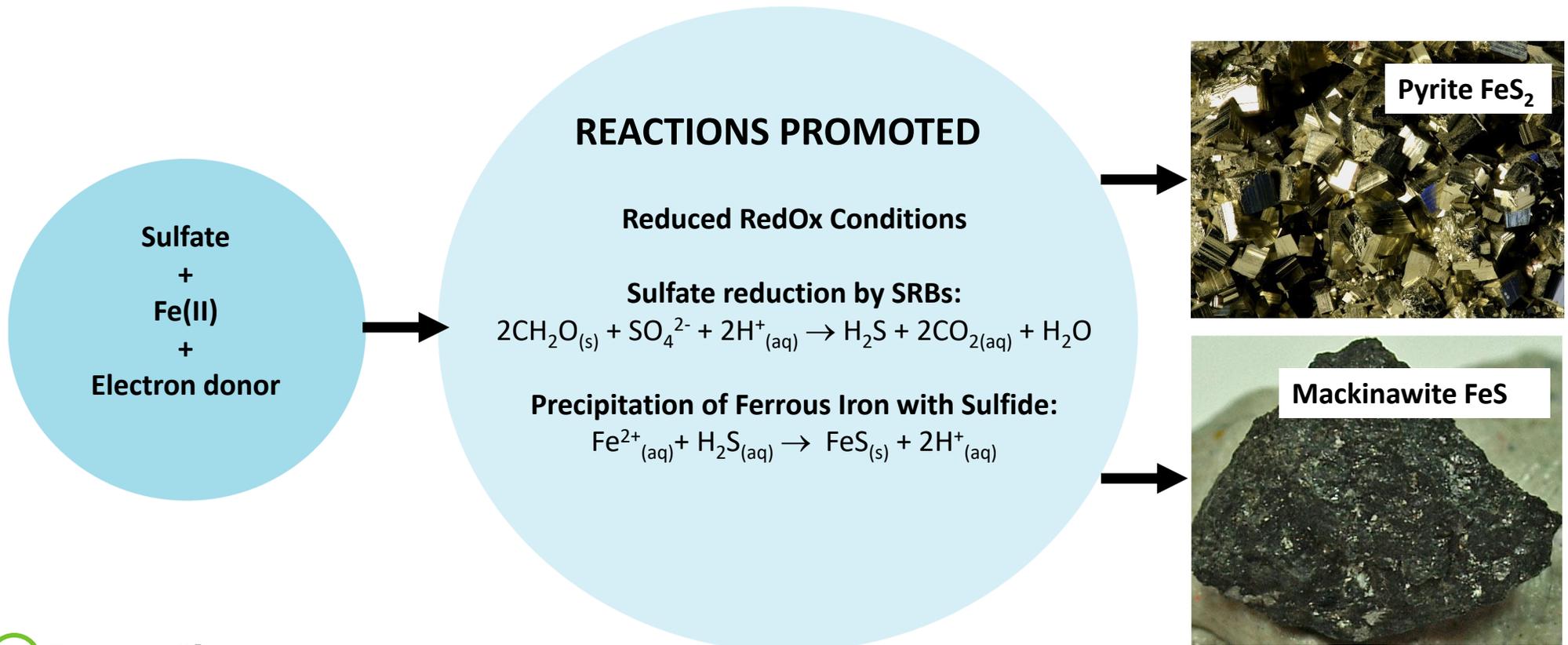
	Feb 2007 (Max Inflowing Conc.)	Oct 2017 (Most Recent Data)
Influent concentrations:		
CT (ppb)	2,700	689
CF (ppb)	120	34
DCM (ppb)	ND (<5)	ND (<5)
Simulated effluent concentrations:		
CT (ppb)	477	122
CF (ppb)	589	154
DCM (ppb)	5	1
Actual effluent concentrations:		
CT (ppb)	33	44
CF (ppb)	8	8
DCM (ppb)	ND (<5)	ND (<5)

Likely Contribution from Biogenic Minerals

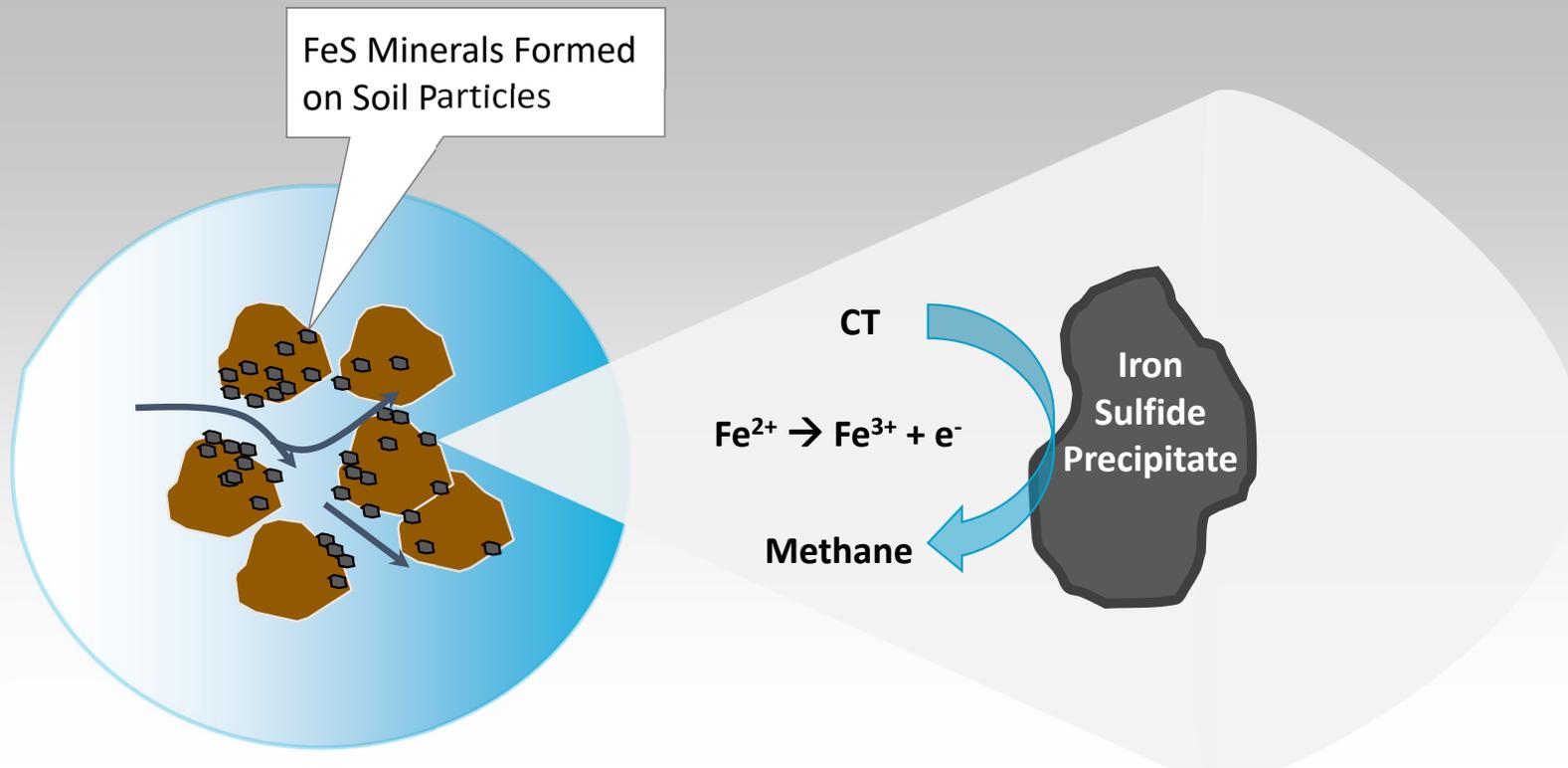
- Biogeochemical transformation refers to processes where contaminants are degraded by abiotic reactions with naturally occurring and biogenically-formed minerals in the subsurface.
- Reactive minerals include iron sulfides (e.g. pyrite, mackinawite, greigite) and oxides (e.g. magnetite)
- **Inflowing sulfate = ~120 mg/L → iron sulfides are likely precipitation products downgradient from PRB → biogeochemical transformation may be an important mechanism to explain extended reactive life**



Mechanisms for Generating Reactive Iron Sulfide Minerals

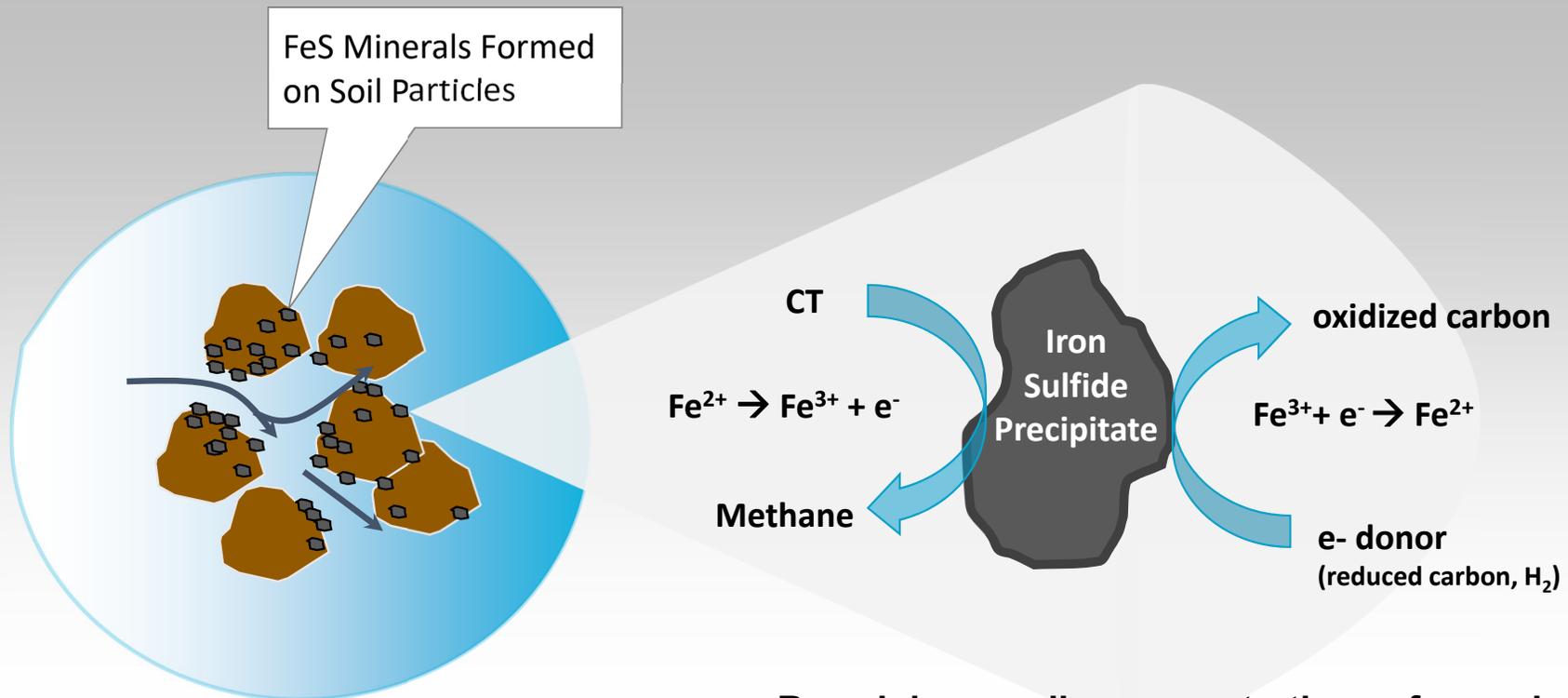


Iron Sulfide Minerals May Serve as a Reservoir of Electrons



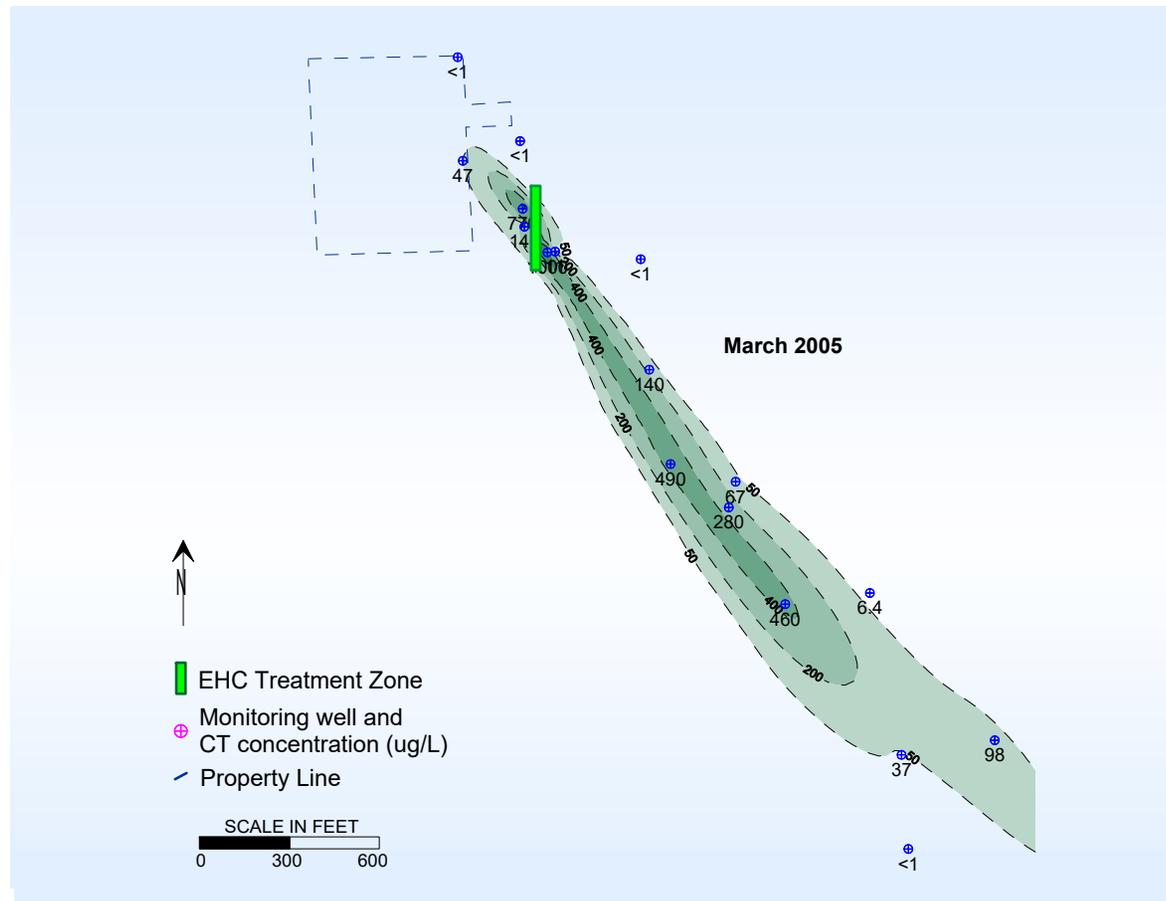
- Fe^{2+} will be oxidized to Fe^{3+} during reaction with chlorinated contaminants

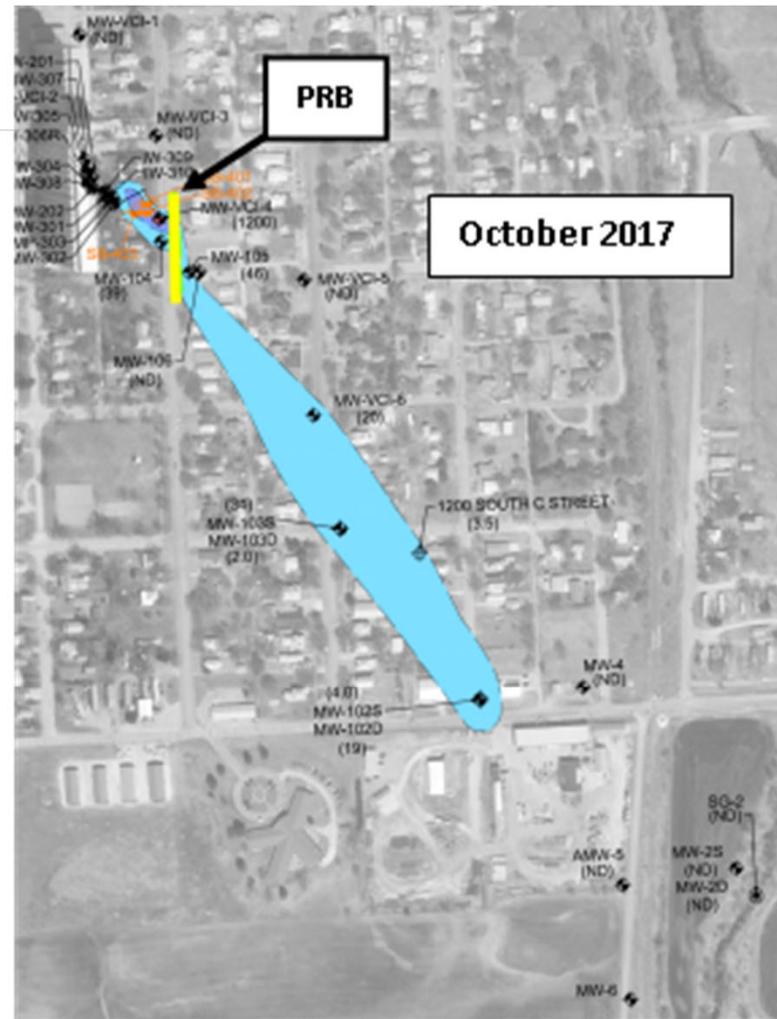
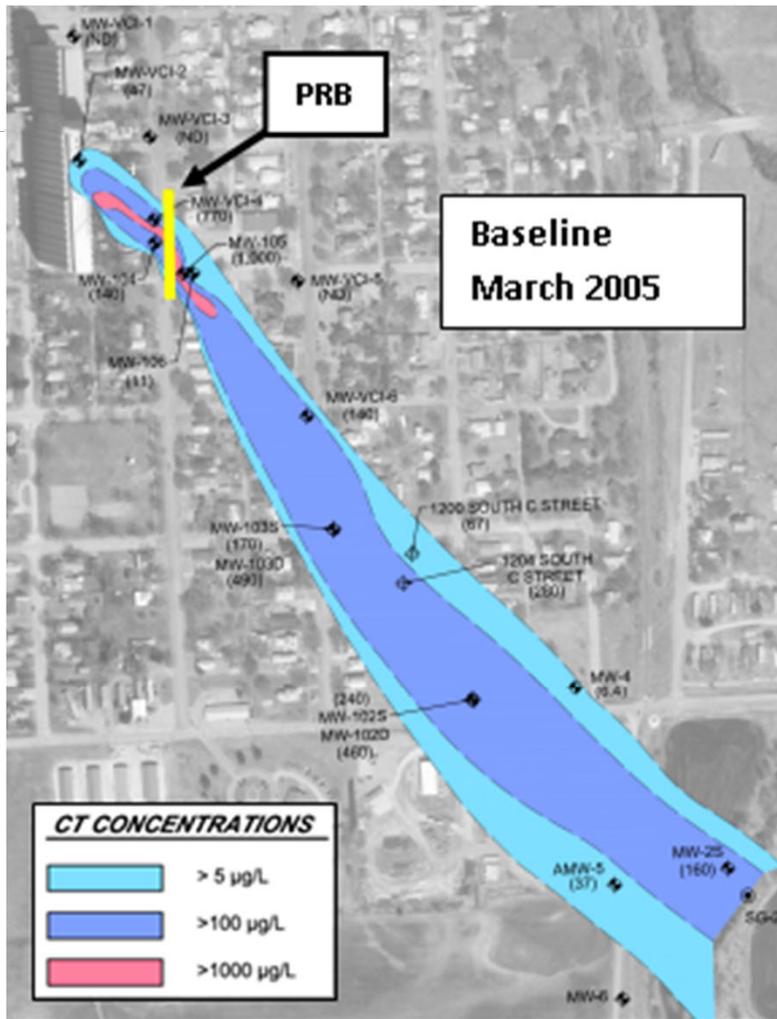
Regeneration of Reactive Minerals – Iron Redox Cycle



- Remaining smaller concentrations of organic carbon and/or natural background TOC (~2 mg/L) may be sufficient to continuously restore Fe^{3+} to Fe^{2+}

CT Concentrations - 5 Years





PRB Economics

Installation costs:

Amendment: 24 tonnes of EHC used in PRB
Product cost = ~\$100,000

Injection: 2 weeks of Geoprobe
Injection Cost = ~\$50,000

Total Fixed Cost: \$150,000

Operating Cost: None

Longevity:

A single application of EHC has remained active for a period of ~12 years before indications of breakthrough started to be observed, continuously supporting >95% removal of CT without the accumulation of catabolites.

PRB treated an estimated ~175,000 m³ GW over its reactive life

Product Cost = ~\$0.57 /m³



This is significantly lower than the pump and treat alternative where just the annual O&M Costs can range from \$ 50K to \$ 300K

**Thank you,
questions are welcome!**

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