Sustainable In-situ Remediation Approach for Arsenic Impacted Groundwater

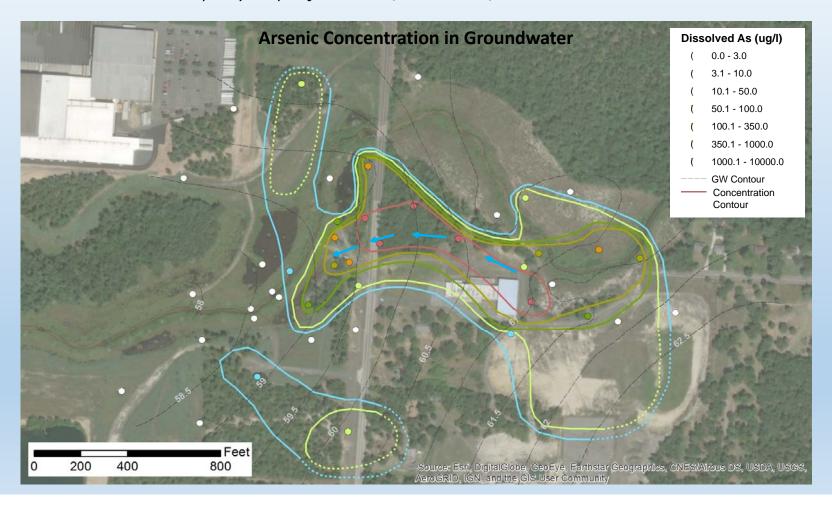
Tricia North, U.S. Army Corps of Engineers, Philadelphia, PA Lily Sehayek, U.S. Army Corps of Engineers, Philadelphia, PA Rick Wilkin, U.S. EPA ORD, Ada, OK Hunter Young, U.S. EPA Region II, New York, NY Diana Cutt, U.S. EPA ORD, New York, NY



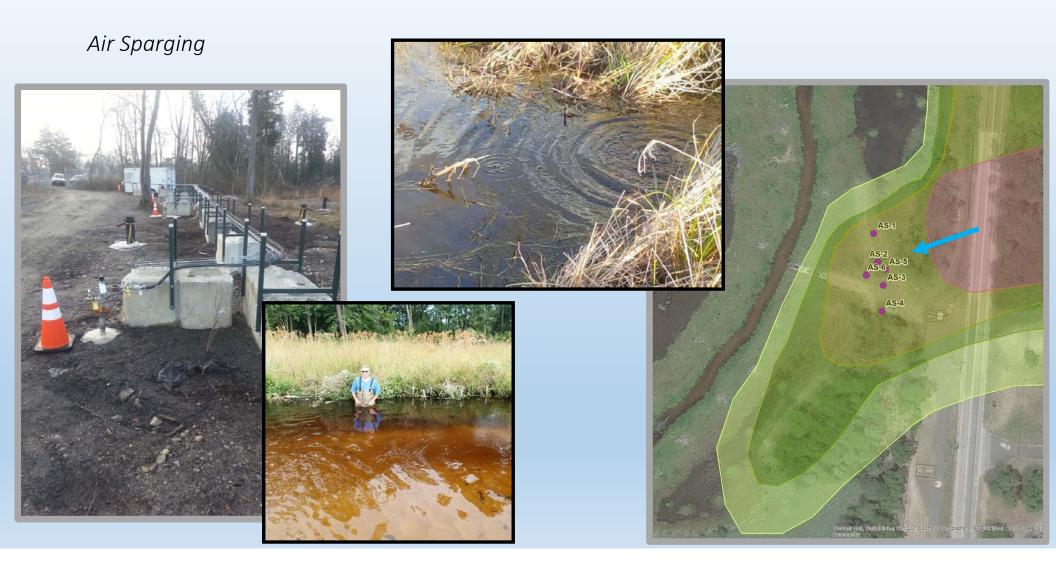


Site background

Vineland Chemical Company Superfund Site, Vineland, NJ



In-situ Immobilization of Arsenic



Soil and Groundwater Characterization

Ambient Conditions

Groundwater

- Anoxic
 - D.O. < < 1 mg/l
 - ORP ≈ -100mV +50mV
- Dissolved arsenic > 1 mg/L
 - As (III) dominant over As (V)
- Dissolved iron ≈ 15-20 mg/L
- pH $\approx 4.5-6$

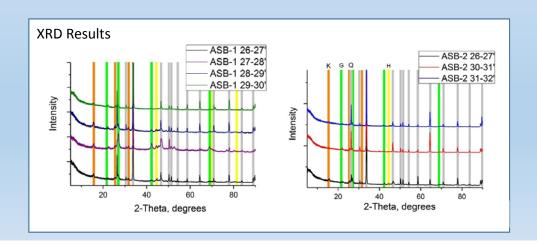
Soil

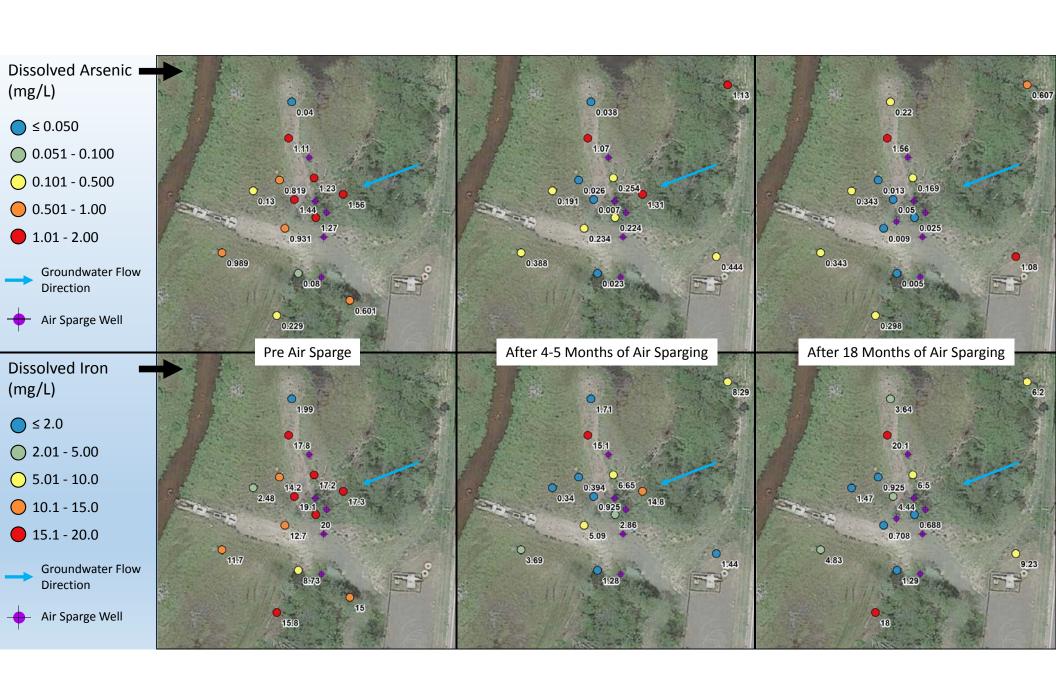
- Iron minerals in soil: goethite, hematite
 - Other minerals: quartz, kaolinite
- High arsenic concentrations coincide with high iron concentrations
- Arsenic (III) sorbs to iron oxides

Air Sparge Conditions

Groundwater

- Aerobic
 - D.O. → solubility (>10 mg/L)
 - ORP: increased to > 300 mV
- Dissolved arsenic reduced to < 0.01 mg/L
 - As (III) dominant over As (V)
- Dissolved iron reduced to as low as 0.01 mg/L
- pH: stable to slight increase





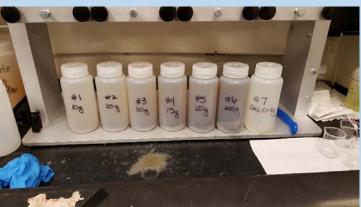
Study Goals

- Identify processes responsible for insitu immobilization of arsenic by air sparging
- Identify optimal conditions for arsenic immobilization
- Develop a numerical tool that can predict arsenic removal under field conditions

Approach

- Laboratory sorption tests using site soil and groundwater
 - Monitor As/Fe changes in batch/column tests
- Geochemical modeling with calibration to laboratory data
- Model verification to field data under anaerobic and air sparge conditions







Geochemical Modeling Approach

- PHREEQC version 3 and wateq4f data base
- Sorption of arsenic to iron oxides
 - Hydrous ferric oxide (HFO) surface complexation model from Dzombak and Morel (1990)
 - Specific Surface Area = 600 m²/g
 - Weak site density = 0.2 moles per mole of iron
 - Mass set by decrease in dissolved Fe plus small percentage of Fe in soil
- Kinetic oxidation of Fe (II) to Fe (III)

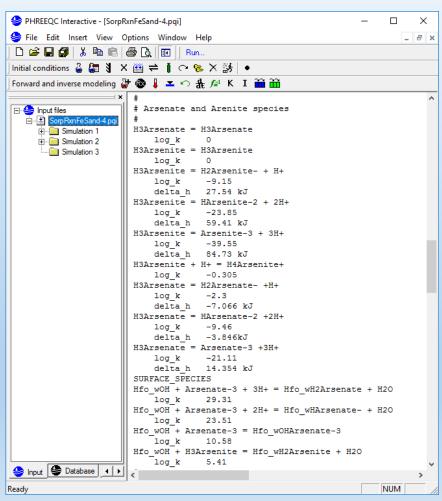
$$rate = -k_{hom}[Fe(II)][O_2][H^+]^{-2} - k_{het}[Fe(III)][Fe(II)][O_2][H^+]^{-1}$$

$$k_{hom} = 8.4 \text{E} - 14 \text{ mol/L/sec*}$$

$$k_{het} = 9.5 \text{E} - 04 \text{ L/mol/sec*}$$

- Degassing of CO₂
- NOT modeling As (III) oxidation to As (V)
 - Kinetics are slow under ambient conditions





Model Calibration Results

Assumptions:

- Mass of freshly precipitated Fe modeled as HFO sorption surface
- 2% 5% Fe in soil modeled as sorption surface (batch tests)
 - Less for column tests (< 0.1%)
- D.O. = 0.2 mg/l 0.8 mg/l
- CO₂ degassing: 10% 60% of initial concentration

10

5

0

10

Measured Fe (mg/L)

20

9:36

Column 1 = Low Fe Sand

Column 2 = High Fe Sand

10:48

12:00

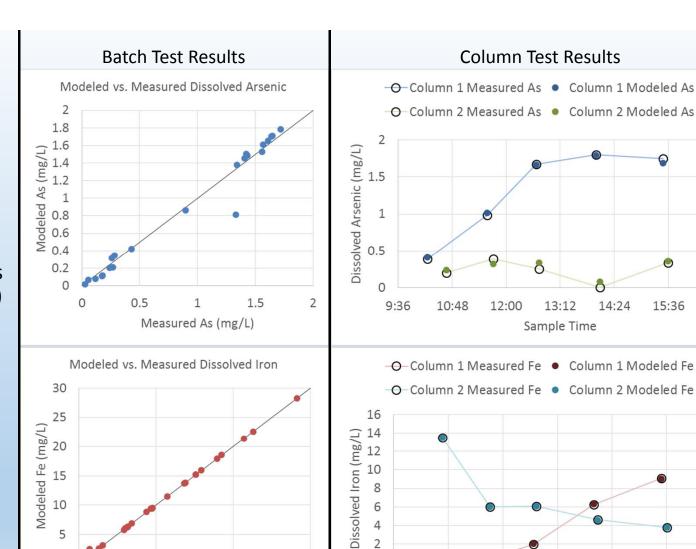
13:12

Sample Time

14:24

15:36

16:48



14:24

15:36

16:48

Model Application to Field: Ambient Conditions

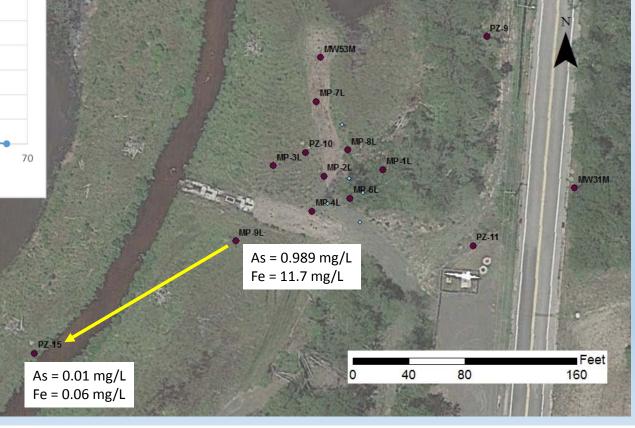


Groundwater flow between MP-9L and PZ-15

Distance = 165 ft
Average Groundwater Flow Velocity = 2.5 ft/day
Travel Time = 66 days

pH = 5.8 D.O. = 0.1 mg/L All precipitated Fe + 1% Fe in soil = HFO sorption surface

Model Calculated Fe @ PZ-15 = 0.044 mg/L Model Calculated As @ PZ-15 = 0.02 mg/L



Model Application to Field: Air Sparging

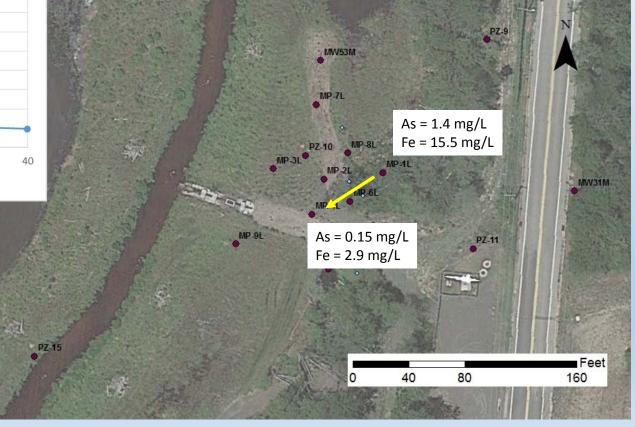


Groundwater flow between MP-1L and MP-4L

Distance = 50 ft Average Groundwater Flow Velocity = 2.5 ft/day Travel Time = 20 days

pH = 5.5 D.O. = 2.0 mg/L All precipitated Fe + 1% Fe in soil = HFO sorption surface

Model Calculated Fe @ MP-4L = 3.0 mg/L Model Calculated As @ MP-4L = 0.14 mg/L



Findings

- Arsenic sorbs to freshly precipitated iron
 - Accounts for approx. 80% of arsenic sorption with remaining arsenic sorbing to Fe oxides in the soil
 - As (III) does not have to oxidize to As (V) to sorb
- Iron oxidation controlled by pH & D.O.
 - Optimal operating conditions -> NOT instantaneous precipitation
- pH controlled by iron chemistry and CO₂ degassing

