

Capillary Rise Study

Interactive Visualizations of 5 Million Sensor Measurements of the Capillary Fringe Lead to an Optimized Soil Remedy



| | A | B | C | D | E | F | G | H | I | J | K | L | M | N | O | P | Q | R | S |
|---------|---|---|---|--------|-------|--------|---|--------|--------|--------|--------|---------|---|--------|--------|---------|---------|---------|---|
| 15-09-1 | 2 | A | 1 | -10.5 | 0.083 | 10.881 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 5.58827 | |
| 15-09-1 | 2 | A | 2 | -47.35 | 0.031 | 8.83 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 4.52727 | |
| 15-09-1 | 2 | A | 3 | -11.17 | 0.005 | 8.458 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 5.13827 | |
| 15-09-1 | 2 | A | 4 | -8.7 | 0.043 | 7.452 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 2.12827 | |
| 15-09-1 | 2 | A | 5 | -9.3 | 7999 | 6.536 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 1.39827 | |
| 15-09-1 | 2 | A | 6 | -7.4 | 7999 | 5.51 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 0.18727 | |
| 15-09-1 | 2 | B | 1 | -10.5 | 0.076 | 10.846 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 5.52227 | |
| 15-09-1 | 2 | B | 2 | -48.47 | 0 | 9.788 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 4.42827 | |
| 15-09-1 | 2 | B | 3 | -8.3 | 0.03 | 8.629 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 3.30827 | |
| 15-09-1 | 2 | B | 4 | -8.87 | 0.043 | 7.89 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 2.36727 | |
| 15-09-1 | 2 | B | 5 | -9.5 | 0.036 | 6.612 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 1.28627 | |
| 15-09-1 | 2 | B | 6 | -7.2 | 7999 | 5.52 | 1 | 22.337 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 0.18727 | |
| 15-09-1 | 1 | A | 1 | -11.6 | 0.116 | 10.648 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 4.49827 | |
| 15-09-1 | 1 | A | 2 | -12.4 | 7999 | 9.676 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 4.51827 | |
| 15-09-1 | 1 | A | 3 | -5.7 | 7999 | 8.482 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 3.52827 | |
| 15-09-1 | 1 | A | 4 | -5.9 | 7999 | 7.452 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 2.29827 | |
| 15-09-1 | 1 | A | 5 | -4.1 | 7999 | 6.523 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 1.36827 | |
| 15-09-1 | 1 | A | 6 | -5.6 | 7999 | 5.499 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 0.34827 | |
| 15-09-1 | 1 | B | 1 | -12.95 | 0.102 | 10.833 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 4.60827 | |
| 15-09-1 | 1 | B | 2 | -11.2 | 7999 | 9.786 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 4.60827 | |
| 15-09-1 | 1 | B | 3 | -7.6 | 7999 | 8.521 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 3.56827 | |
| 15-09-1 | 1 | B | 4 | -5.6 | 7999 | 7.488 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 2.33827 | |
| 15-09-1 | 1 | B | 5 | -4 | 7999 | 6.524 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 1.36727 | |
| 15-09-1 | 1 | B | 6 | -5.7 | 7999 | 5.513 | 1 | 22.481 | 36.517 | 15.815 | 417024 | 2.80805 | 0 | 30.248 | 34.267 | 2.24828 | 5.15803 | 0.35827 | |
| 15-09-1 | 2 | A | 1 | -10.53 | 0.082 | 10.891 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 5.58827 | |
| 15-09-1 | 2 | A | 2 | -47.3 | 0.031 | 8.85 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 4.52727 | |
| 15-09-1 | 2 | A | 3 | -11.2 | 0.005 | 8.459 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 5.13827 | |
| 15-09-1 | 2 | A | 4 | -8.7 | 0.043 | 7.452 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 2.12827 | |
| 15-09-1 | 2 | A | 5 | -9.3 | 7999 | 6.536 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 1.39827 | |
| 15-09-1 | 2 | A | 6 | -7.4 | 7999 | 5.51 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 0.18727 | |
| 15-09-1 | 2 | B | 1 | -10.53 | 0.076 | 10.846 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 5.52227 | |
| 15-09-1 | 2 | B | 2 | -48.47 | 0 | 9.789 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 4.42827 | |
| 15-09-1 | 2 | B | 3 | -8.3 | 0.03 | 8.629 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 3.30827 | |
| 15-09-1 | 2 | B | 4 | -8.8 | 0.043 | 7.89 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 2.36727 | |
| 15-09-1 | 2 | B | 5 | -9.5 | 0.036 | 6.612 | 1 | 22.335 | 36.802 | 15.939 | 416906 | 2.78945 | 0 | 30.248 | 34.267 | 2.55328 | 5.52275 | 1.28627 | |

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Thursday April 12, 2018

AECOM

Big Problems and Little Problems

– BIG PROBLEM

- Regulator required 28 acres of impervious liner above GW plume

– Little Problem

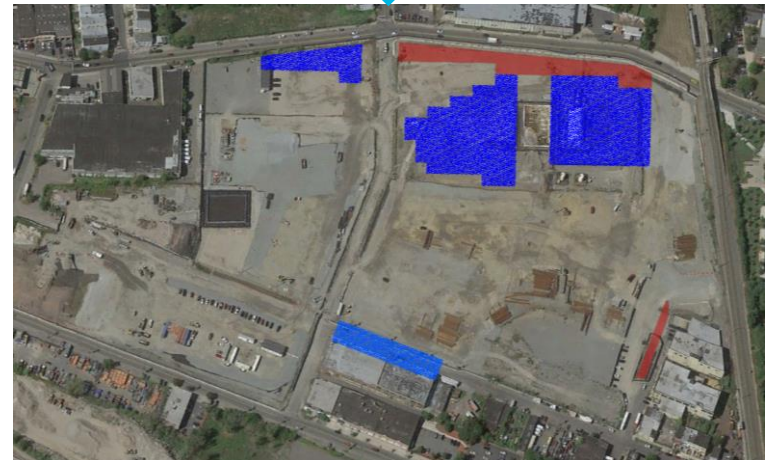
- Field study for alternatives to liner generated a massive amount of difficult to analyze data

– Little Solution

- Create custom interactive data viewer

– BIG SOLUTION

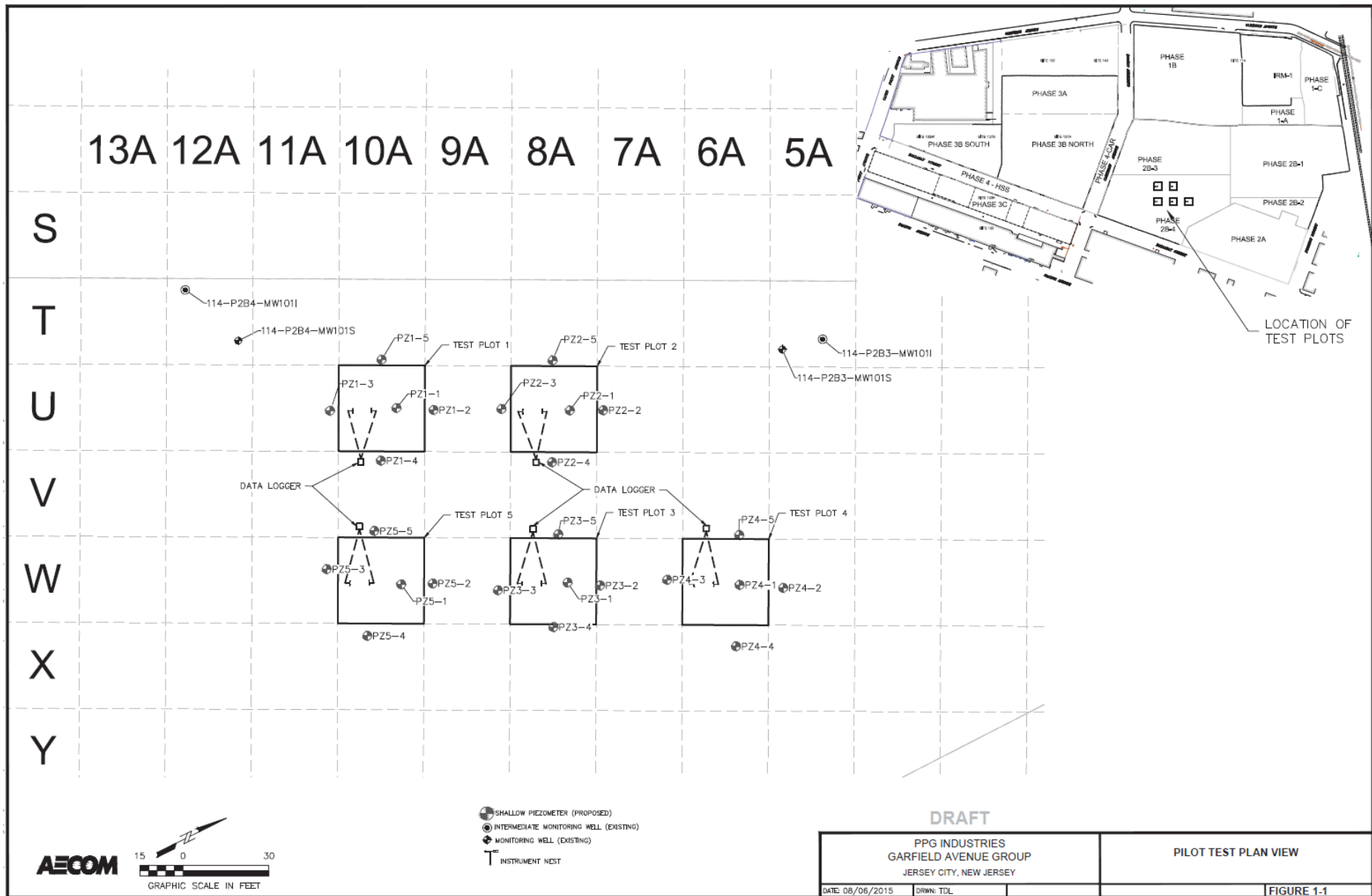
- Regulator accepted 0.8 acres of impervious liner and 3.6 acres of washed stone capillary break



Field Study Objectives

- 1. Determine the height of the capillary fringe in dense grade aggregate (DGA) backfill material at the site.**
- 2. Determine the height of the capillary fringe in topsoil backfill material at the site when placed in sufficient thickness to hydraulically connect with the saturated zone of the capillary fringe.**
- 3. Evaluate the effectiveness of an engineered capillary break on limiting the height of the capillary fringe in backfill material at the site.**

Test Plot Layout



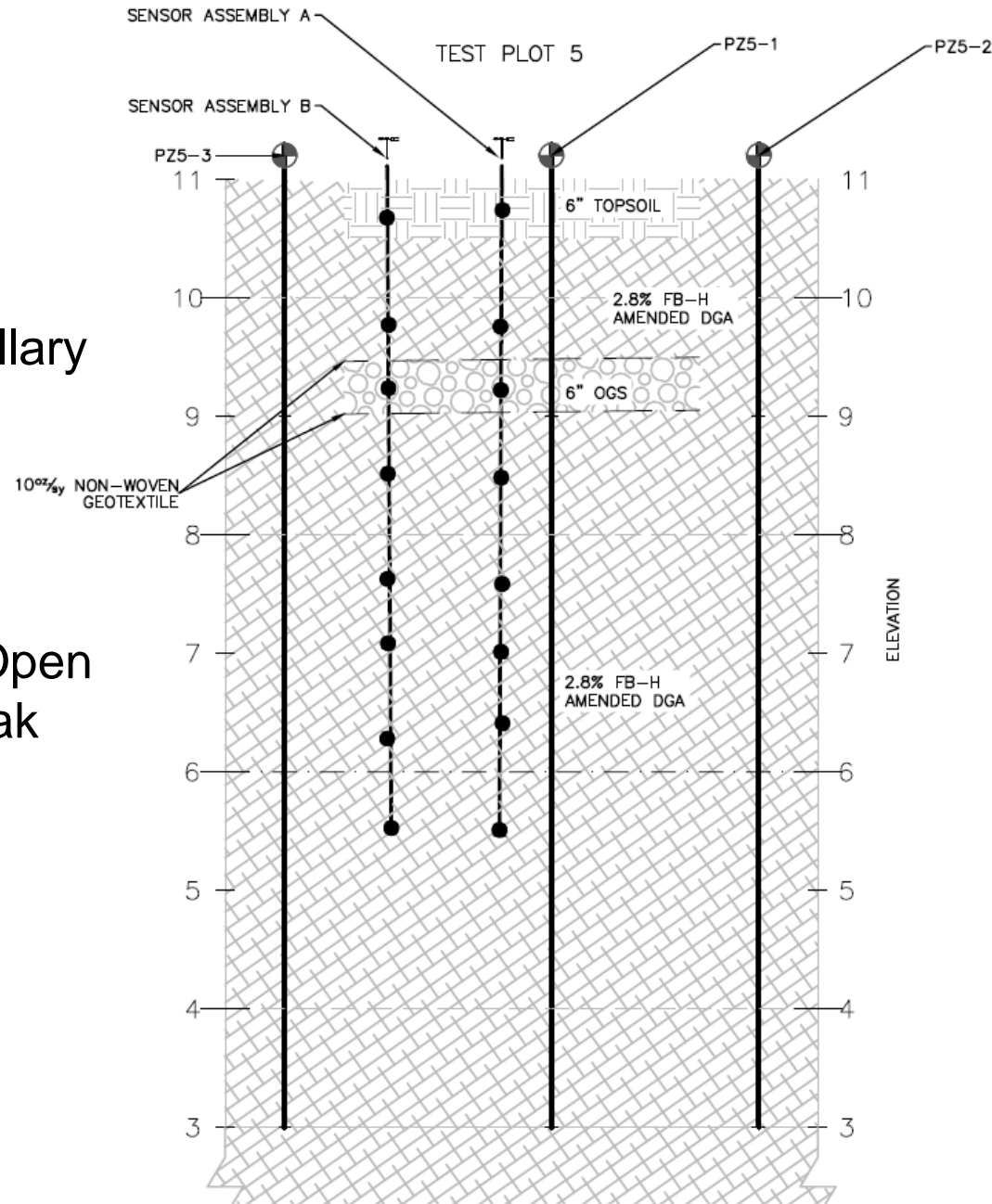
Test Plot Construction

– Test Plot 5

- Amended DGA
- 6" Open Grade Stone Capillary Break from El. 9 to El. 9.5
- 6" of topsoil at surface

– Objective

- Evaluate effectiveness of Open Grade Stone Capillary Break



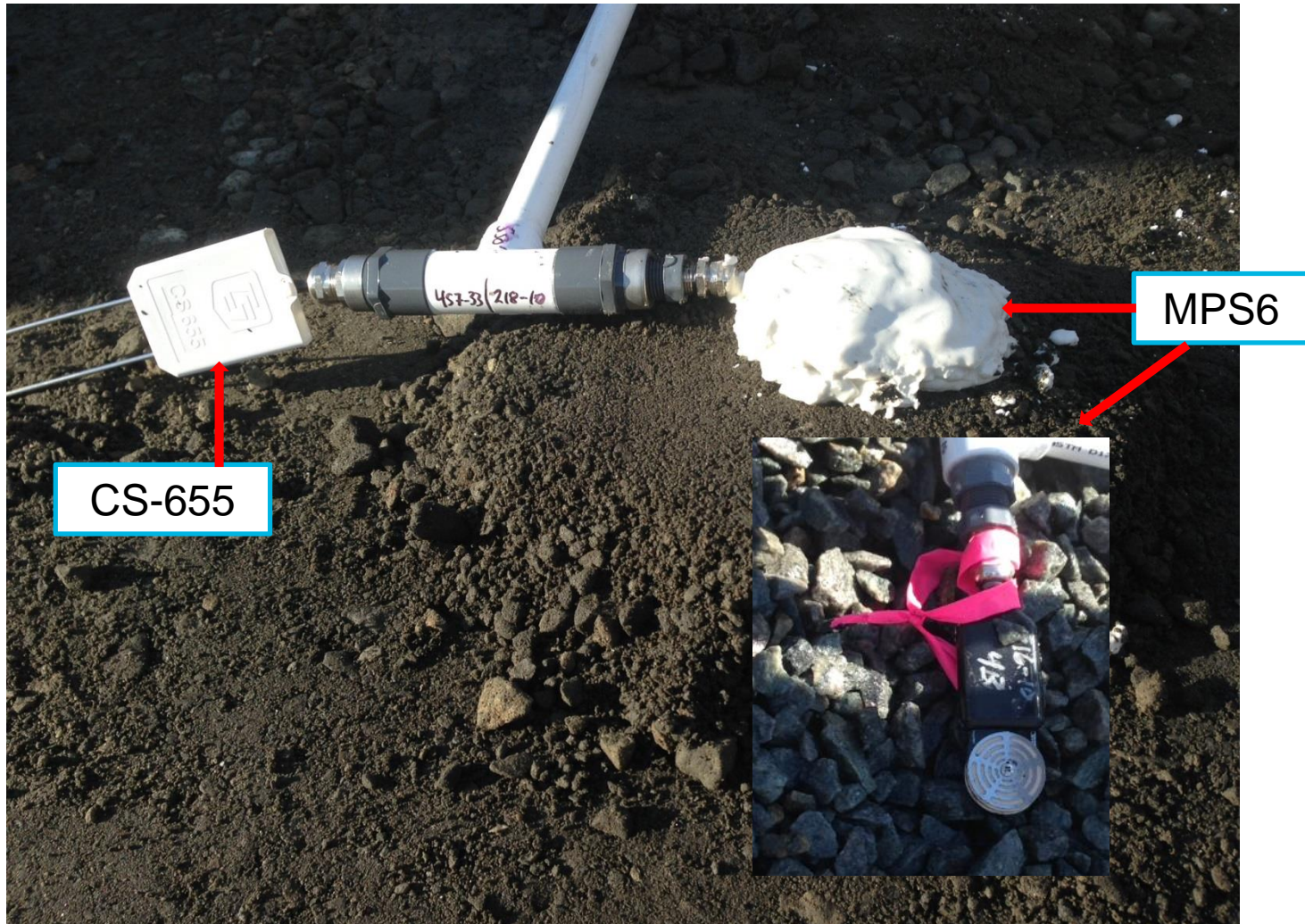
Amended DGA



Capillary Break Layers



Sensor Placement

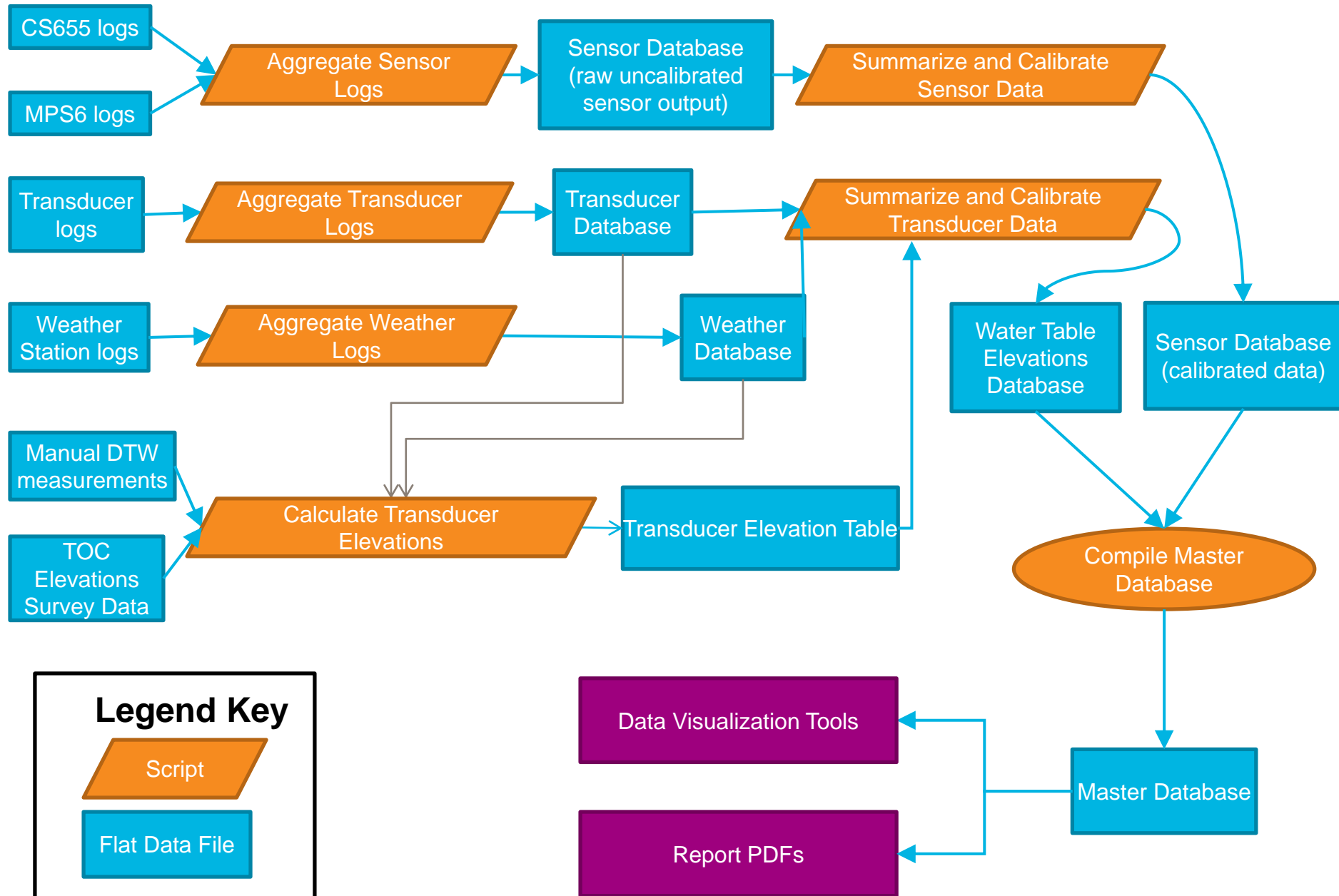


Data Collection Progress

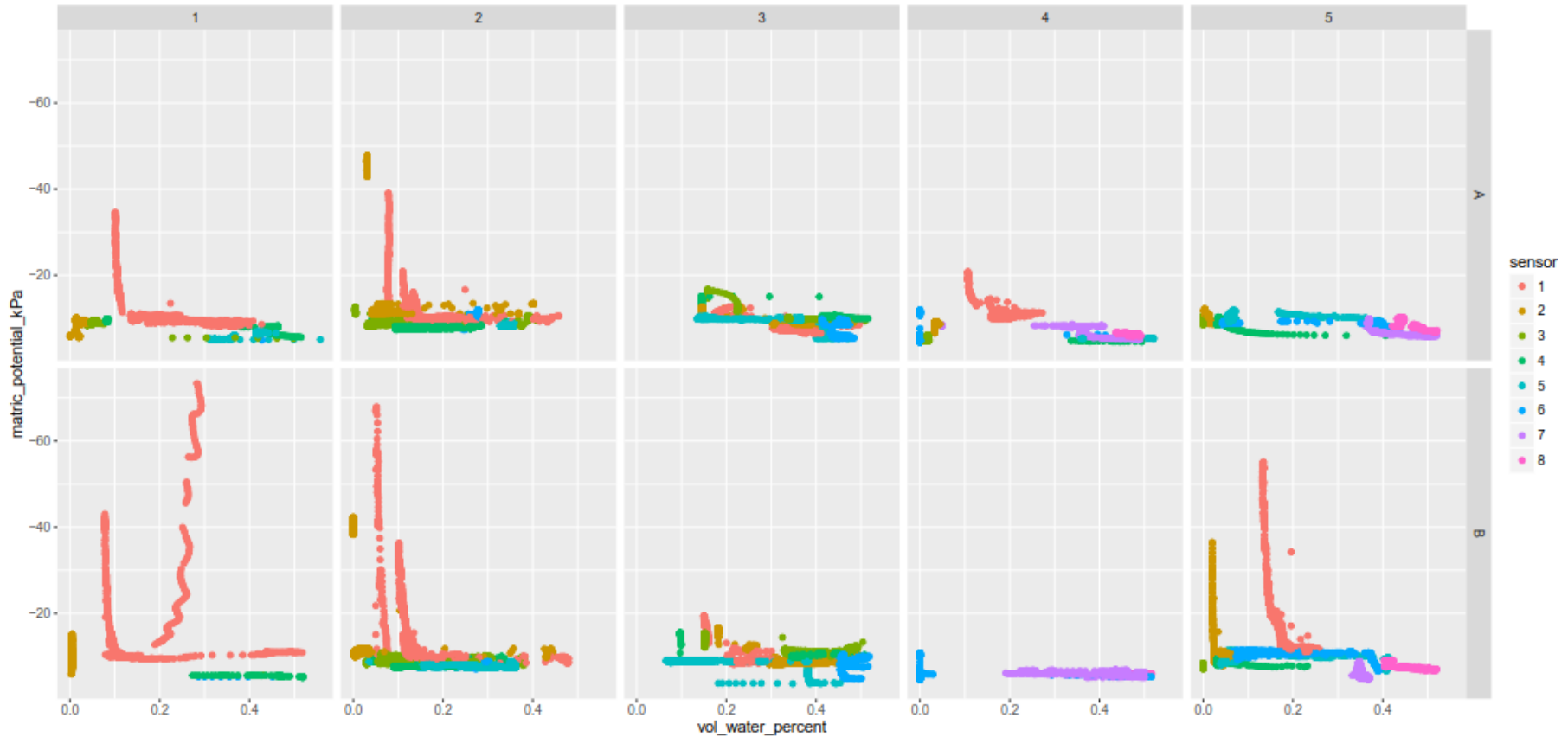
- Sensor Types
 - CS-655 – Volumetric Water Content Sensor
 - MPS-6 – Matric Tension Sensor
 - Water Level Transducers
 - Water Level Transducers in Piezometers
 - Water Level Transducers in Shallow Wells
 - Meteorological

Data Collection and Processing

- 129 sensors in the field recordings readings every hour
 - 5 soil plots (experimental groups)
 - 2 sensor nests per plot
 - 6 or 8 sensors levels per nest
 - 2 sensors per level
 - 5 transducers (piezometers) per soil plot
- Weather station recording 8 values every 15 minutes – used to normalize / interpret transducer data
- 1,410,360 complete records generated
 - 1 record per sensor location per hour

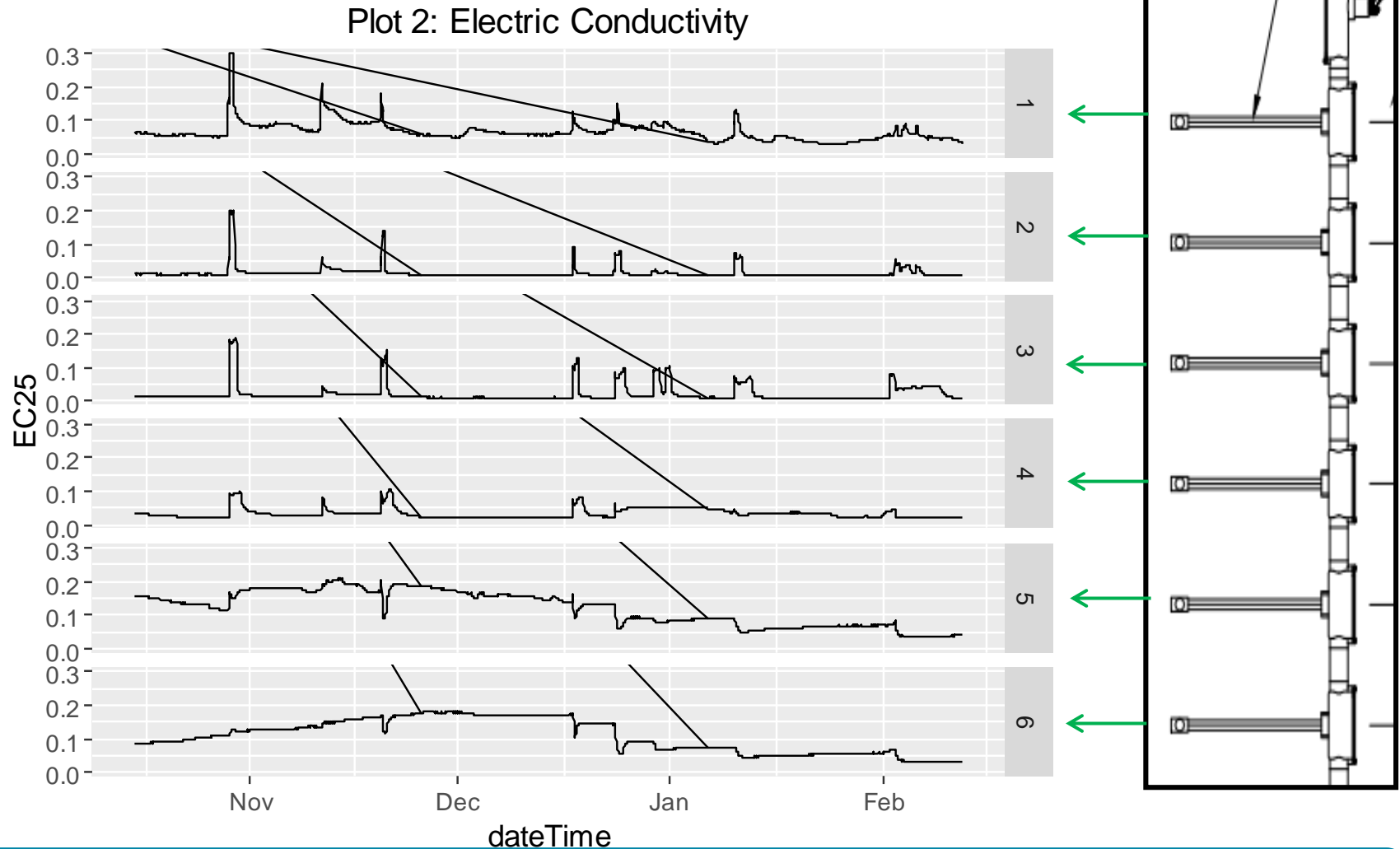


Data Visualization Issues



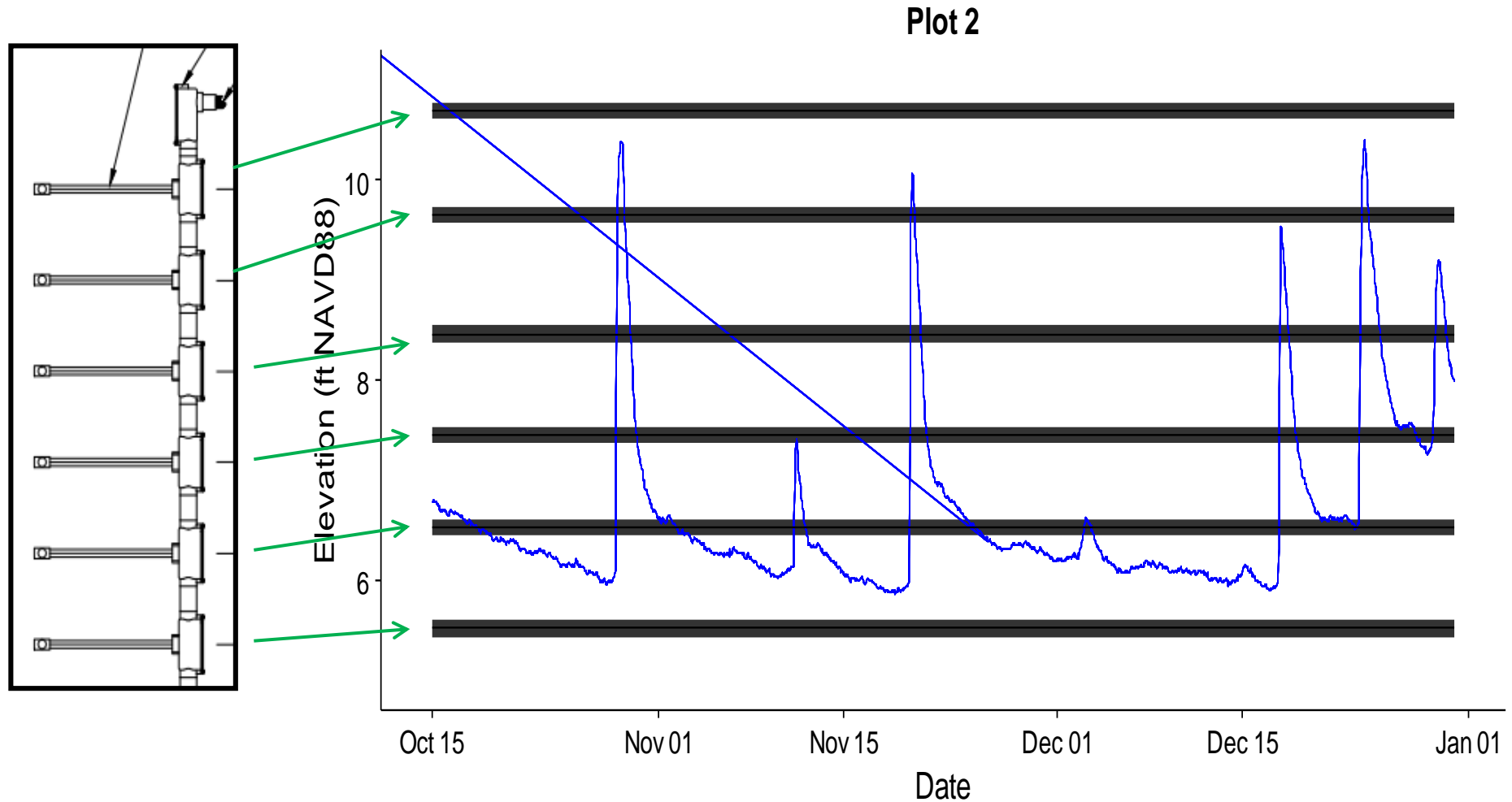
No patterns visible in planned graphics.

Visualization - Sensor Output



Temperature Normalized Electrical Conductivity over Time - Stacked by Sensor Position.

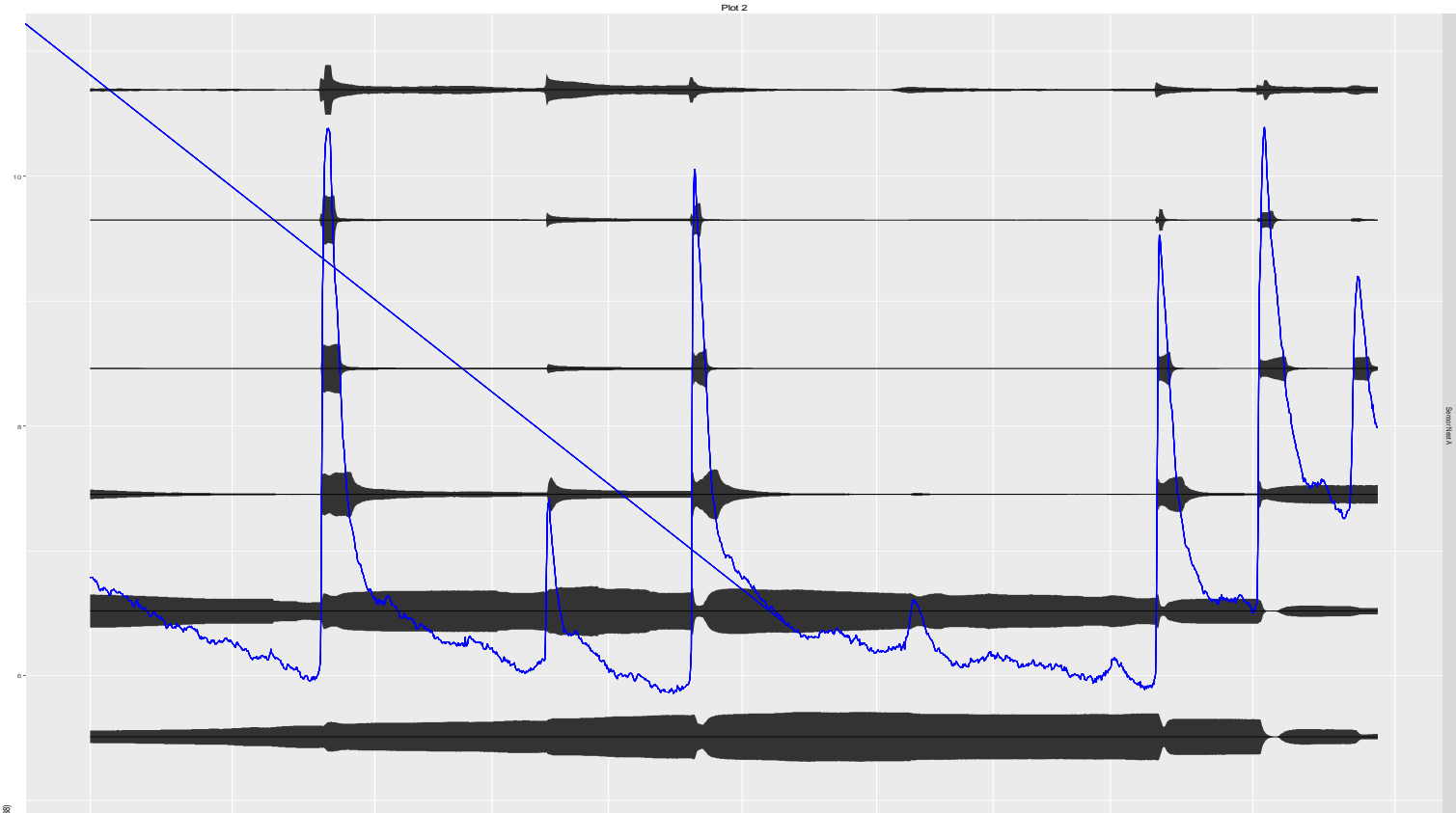
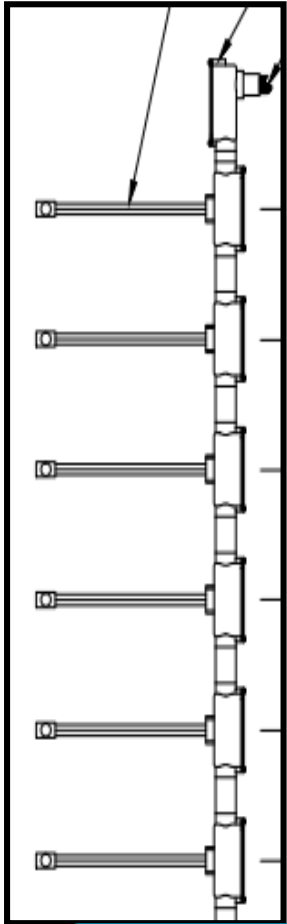
Visualization - Sensor Elevations Relative to the Water Table



Visualization – Sensor Output relative to Groundwater Elevation

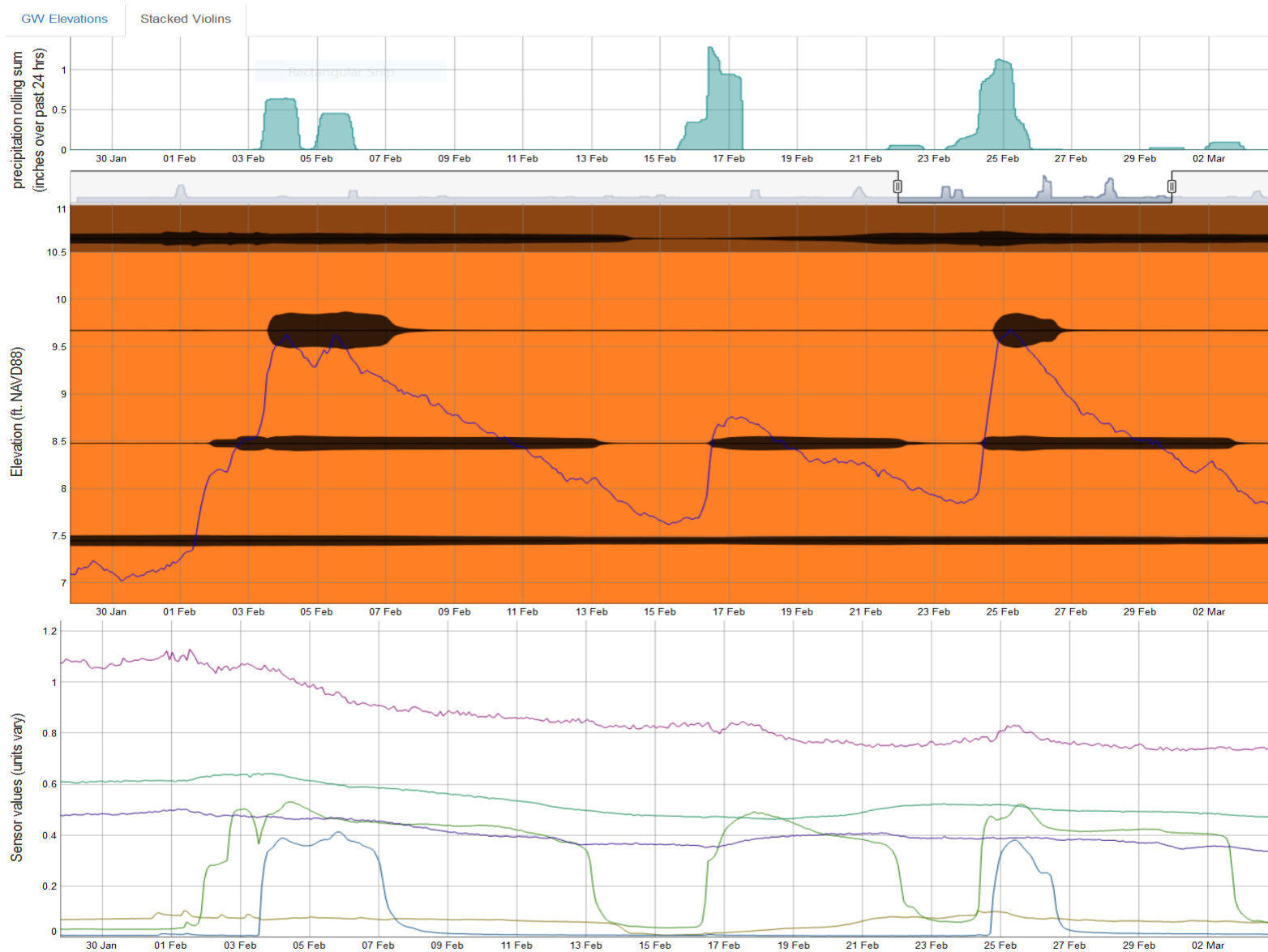
Visualizing four variables in one graph:

- + Time
- + Sensor Value (Violin Plot)
- + Sensor Elevation
- + WT Elevation



Combined Data Visualization

Visualization - Precipitation, GW, and Sensor Data



Interactive Tool

- Allows easy visualization of any variable collected

Data Subsetting Options

Select a soil plot
2

Select a sensor nest
☒ A ☐ B

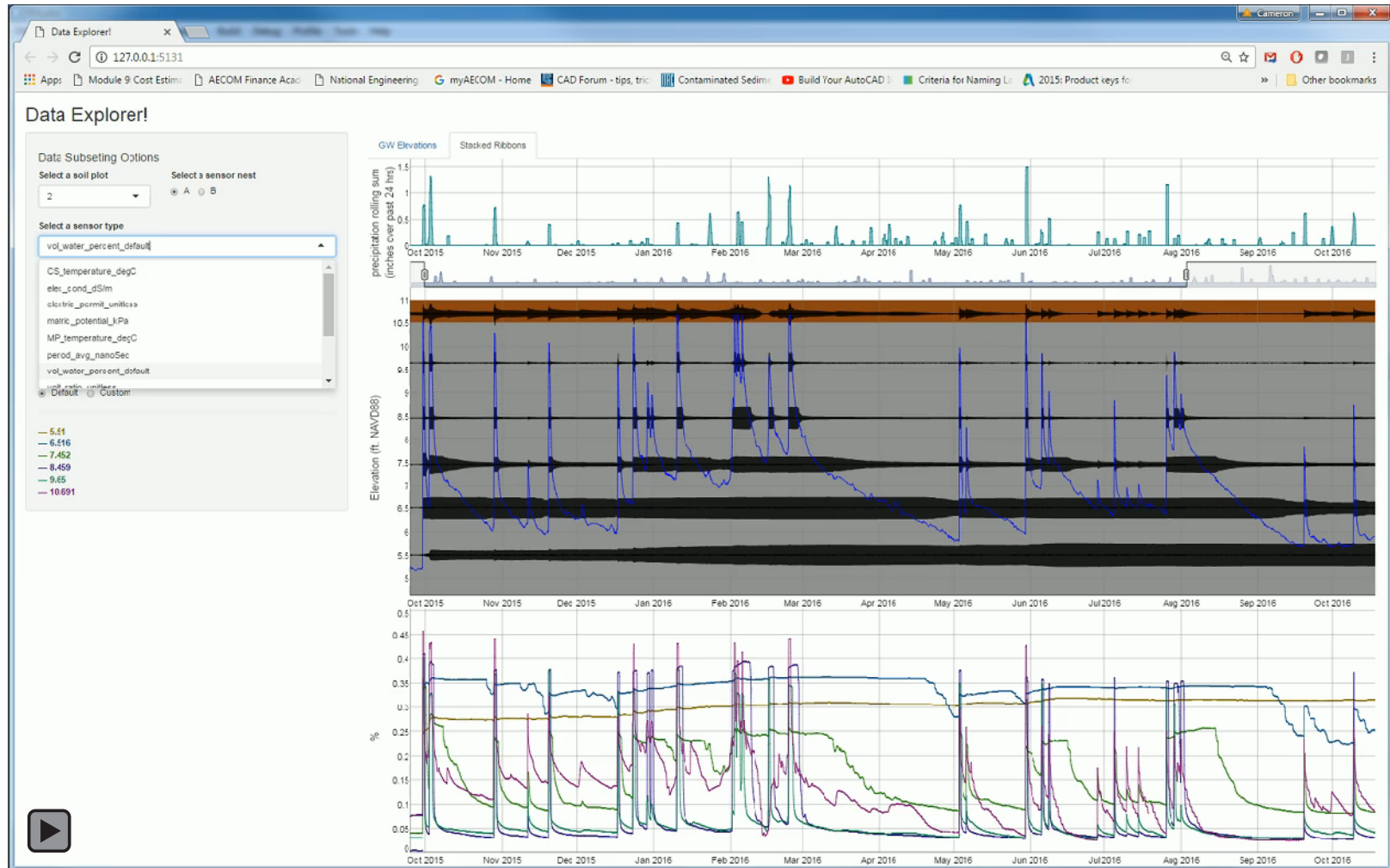
Select a sensor type
vol_water_percent_default

CS_temperature_degC
elec_cond_dS/m
electric_permit_unitless
matric_potential_kPa
MP_temperature_degC
period_avg_nanoSec
vol_water_percent_default
volt_ratio_unitless

☒ Default ☐ Custom

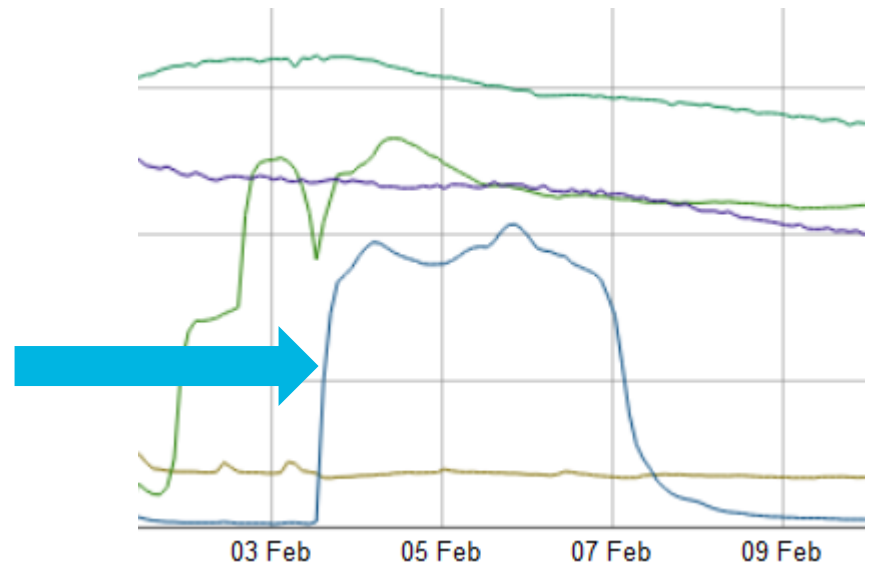
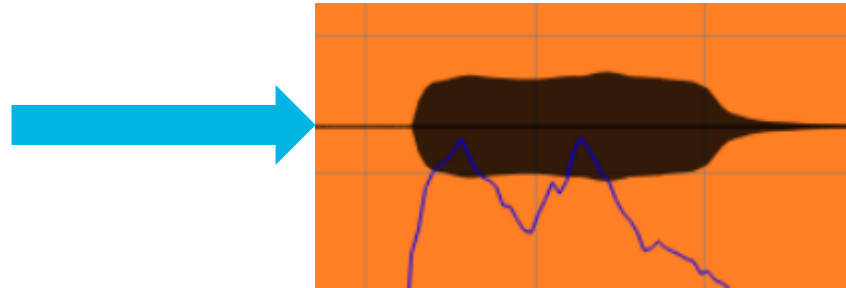
— 5.51
— 6.516
— 7.452
— 8.459
— 9.65
— 10.691

Video of Tool Operation

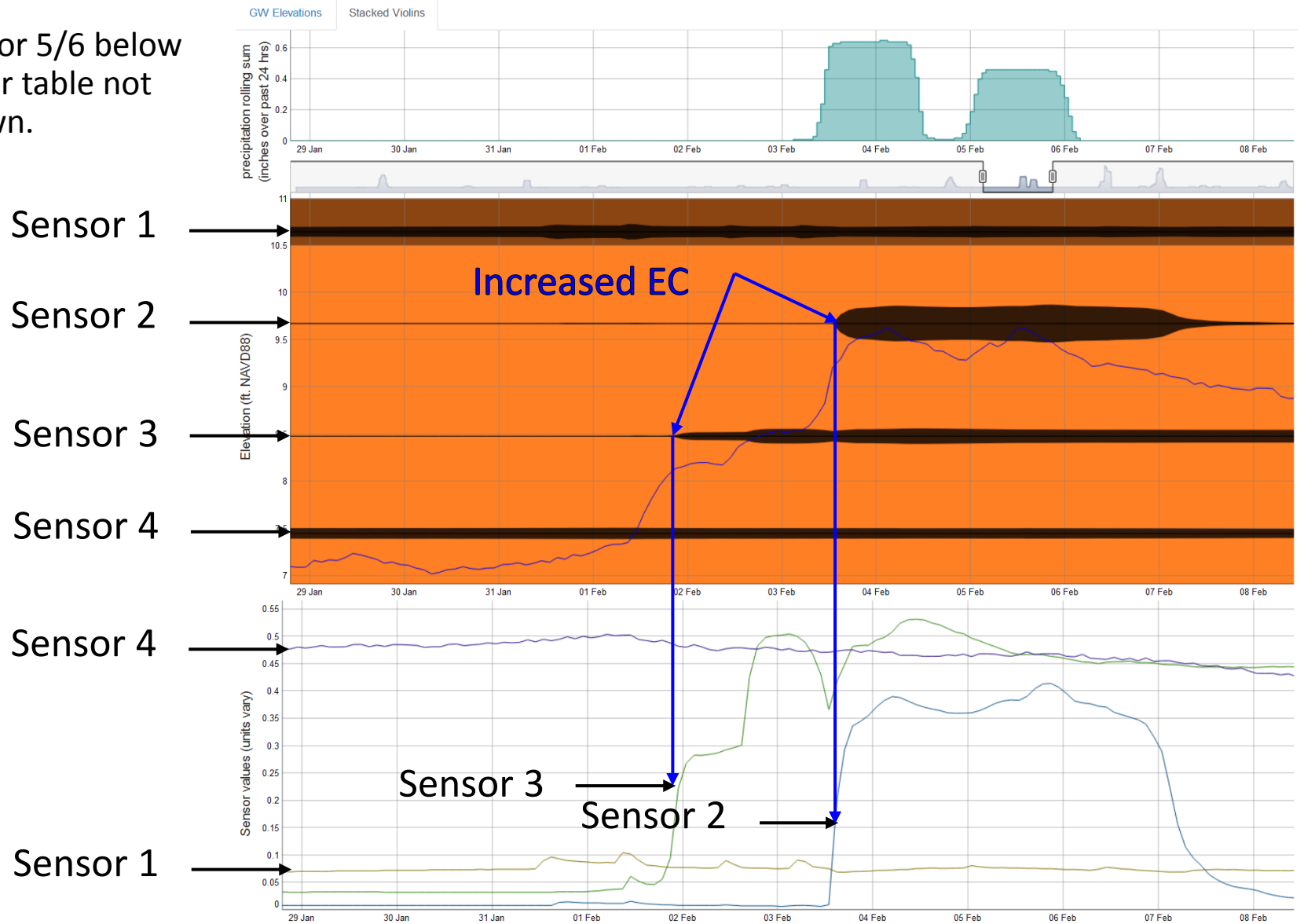


Interpretation – Identify Sustained Sensor Change Above Water Table

- Sustained increases in EC indicate saturation.
- Saturation above the water table means the sensor is in the capillary fringe,

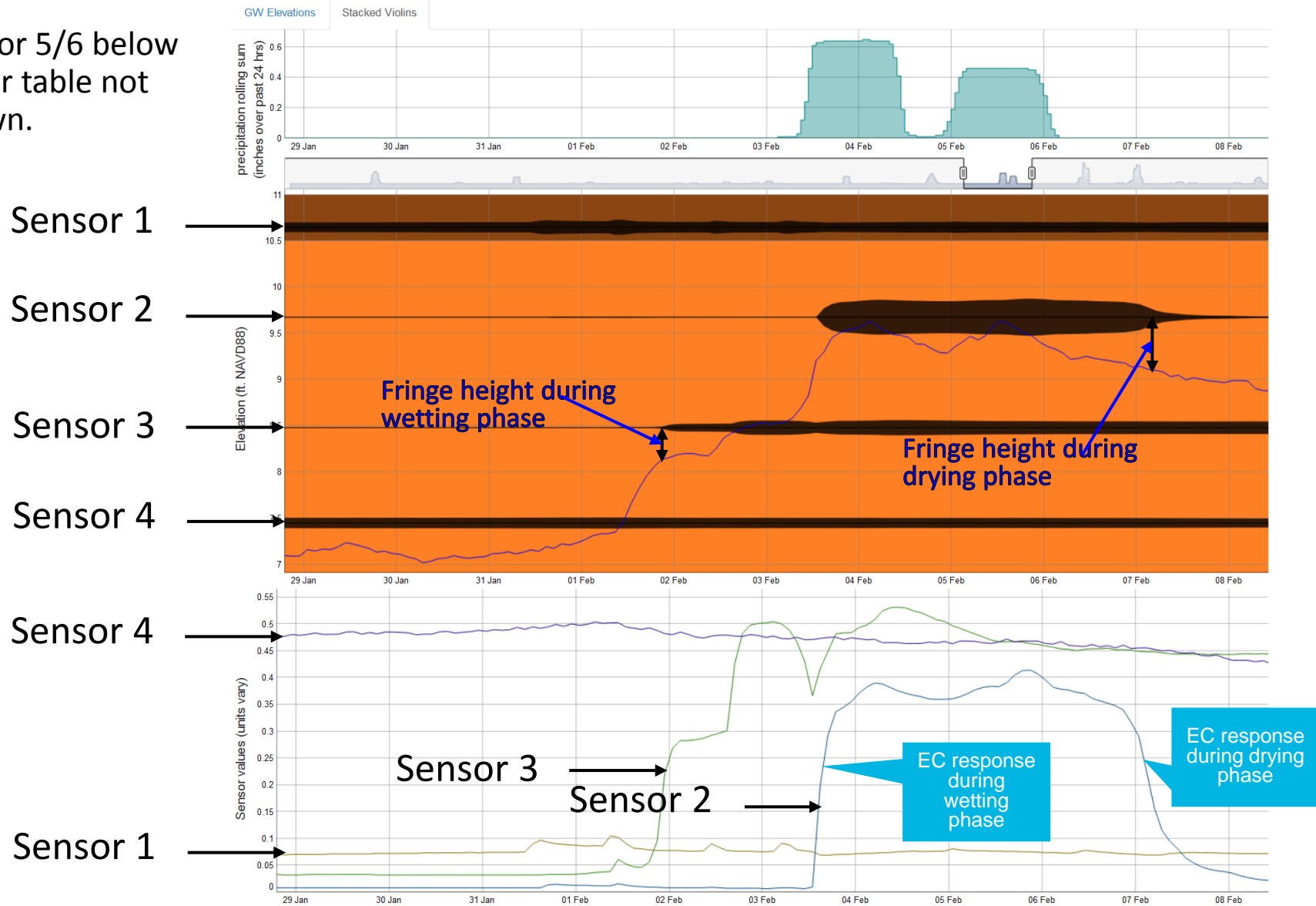


Sensor 5/6 below
water table not
shown.

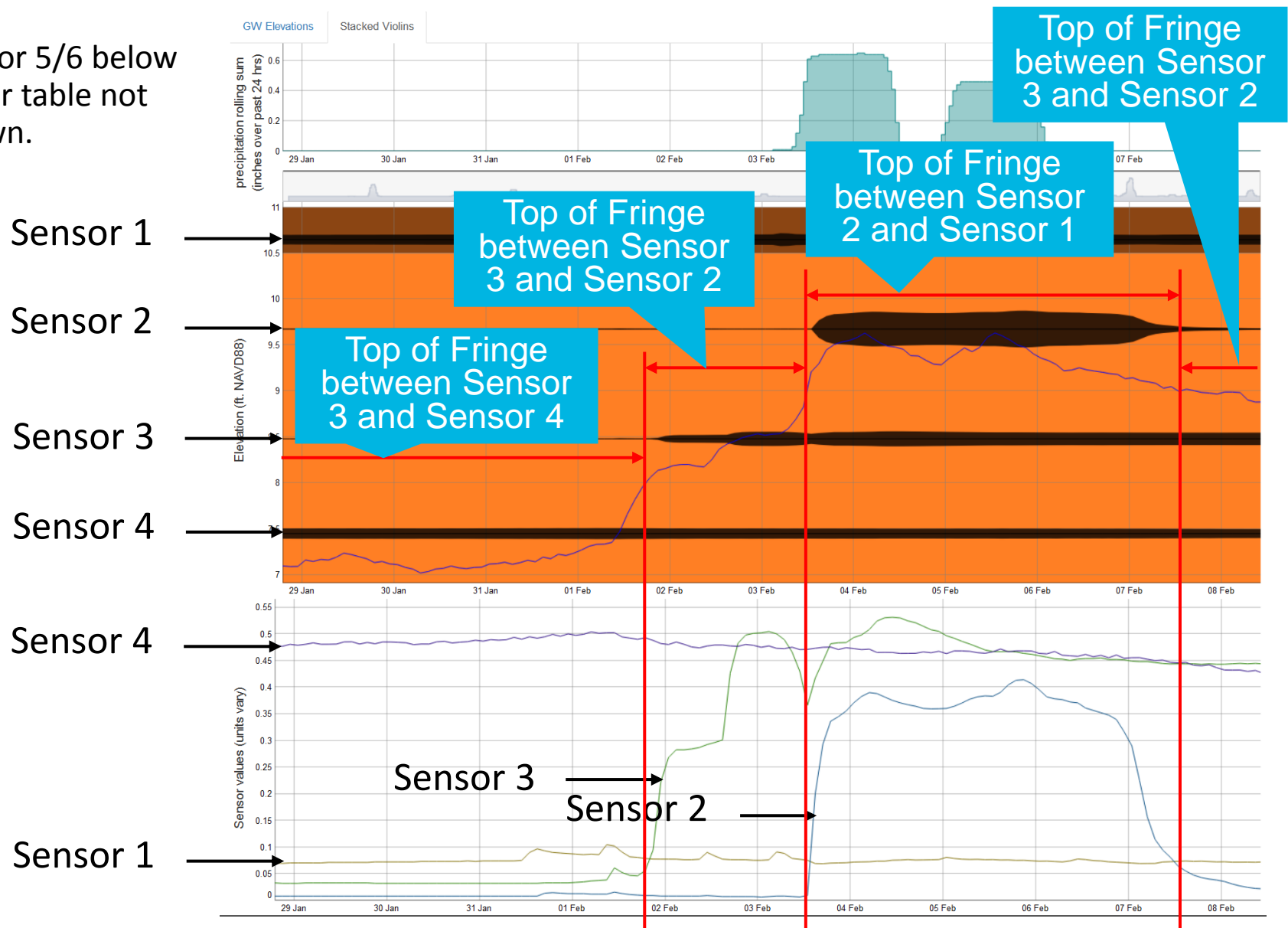


Interpretation - Water Table Changes – Wetting vs. Drying

Sensor 5/6 below water table not shown.

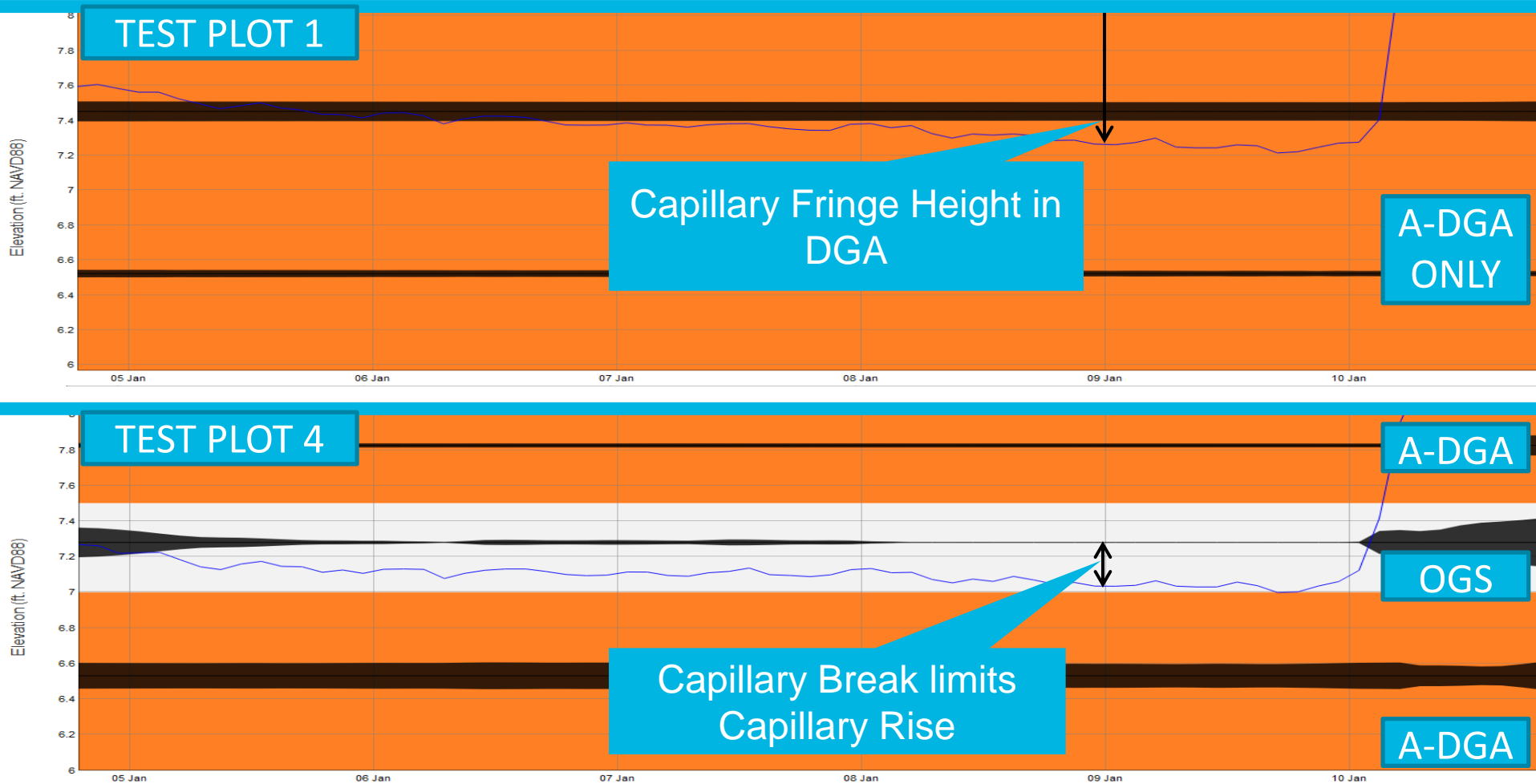


Sensor 5/6 below
water table not
shown.



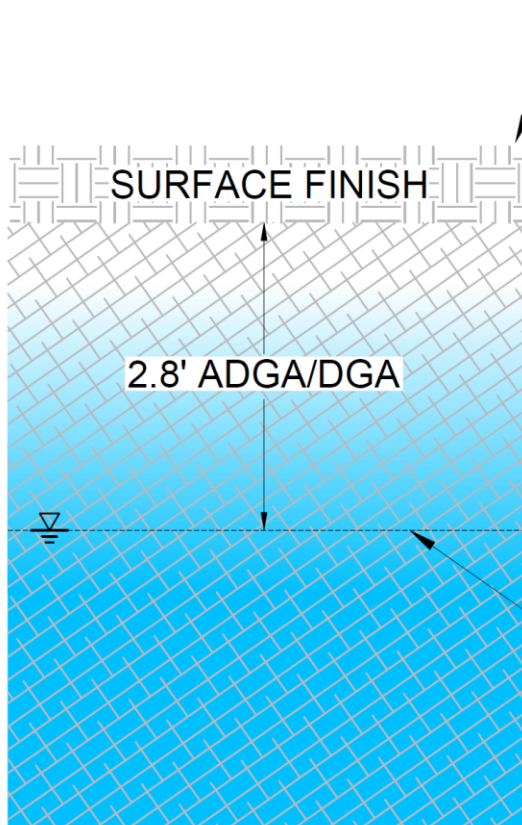
Interpretation - Open Grade Stone Capillary Break

Direct Comparison of Capillary Fringe Height shows Capillary Break Effectiveness

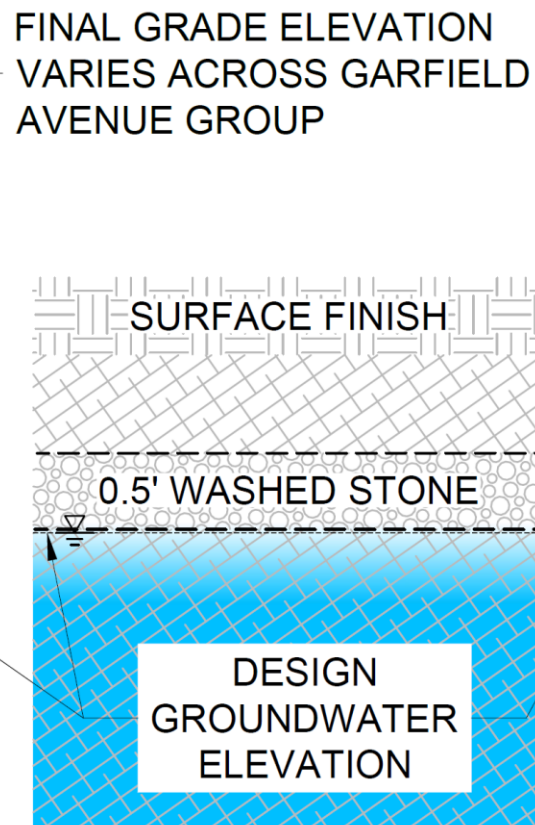


Capillary Break Construction Options

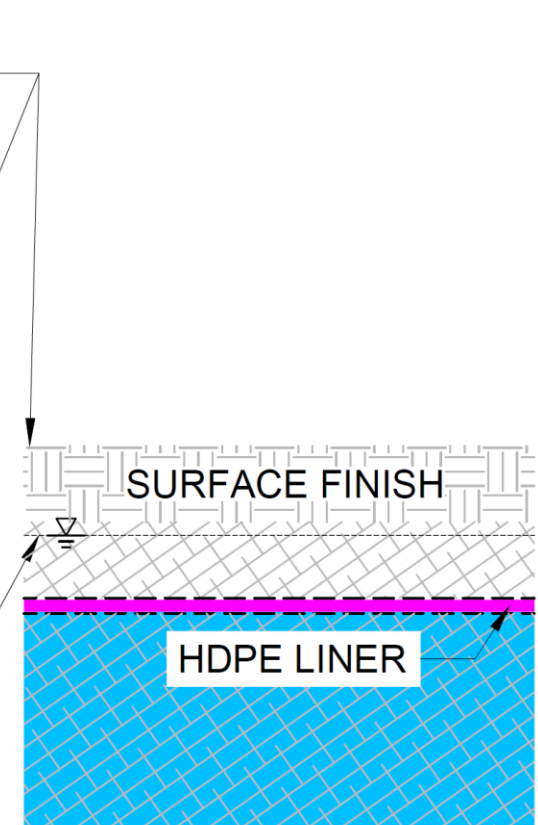
ADGA/DGA CAPILLARY BREAK



WASHED STONE CAPILLARY BREAK



HDPE LINER CAPILLARY BREAK



Big Problem



Big Solution



Questions

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